

# NADim-seminar 2023

## Comparison of deflection measurements with RAPTOR / TSD / FWD

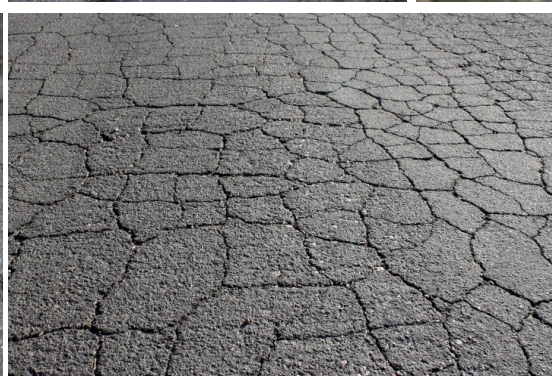
Arman Hamidi

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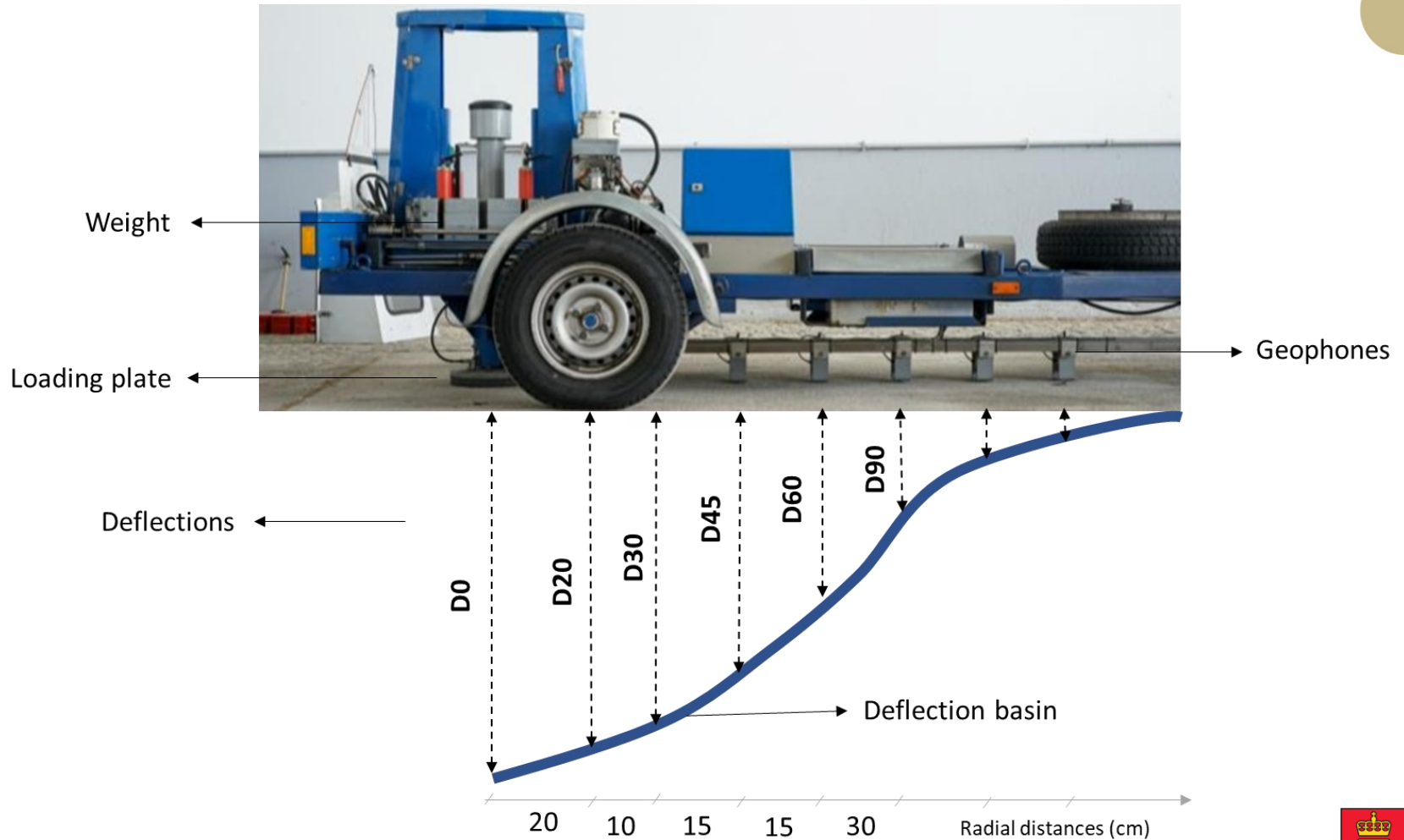
30. November 2023, Oslo

# Pavement Management System

- Two Important questions:
  - WHEN are treatments needed?
  - WHICH treatments should be used?
- Maintenance timing
- Types of distresses
  - Functional
  - Structural



# Falling Weight Deflectometer (FWD)



# FWD versus TSDDs

- Disadvantages of using FWD
  - Discrete measurements
  - Lanes must be closed to traffic
  - Stationary dropping weight
  - Not suitable for network-level evaluations
- Traffic Speed Deflection Devices (TSDDs)
  - Two current types include **TSD** and **Raptor**
- Advantages of using TSDDs
  - Continuous measurements
  - Measuring at traffic speed
  - Resemble the service condition of roads
  - Suitable for network-level evaluations



# Traffic Speed Deflectometer (TSD)

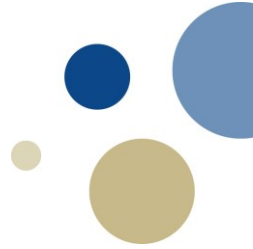
- Doppler laser sensors
- Measures deflection velocity
- Mathematical procedures are used to obtain deflections



# Rapid Pavement Tester (Raptor)

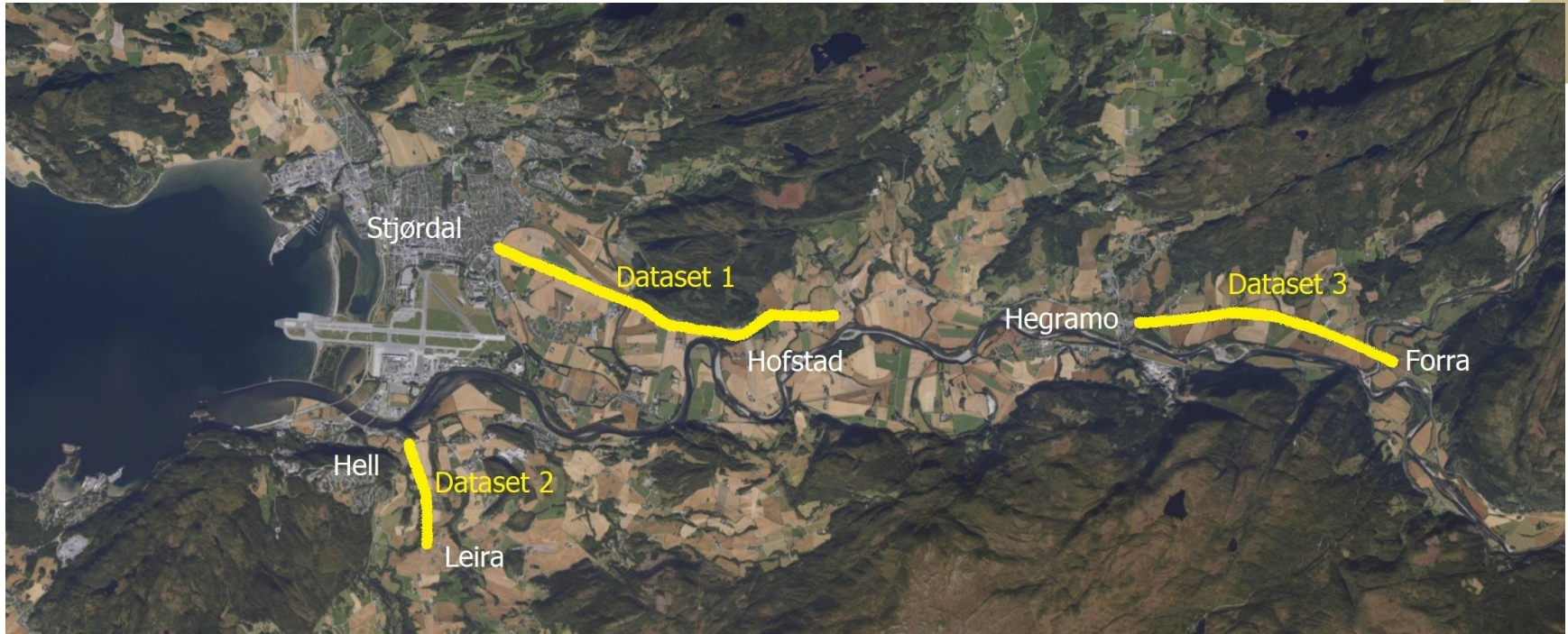
- Line laser sensors
- Image recognition techniques
- Raptor deflection indices (RDIs) are finally converted to equivalent FWD deflections





# Is there any consistency between FWD and TSDDs?

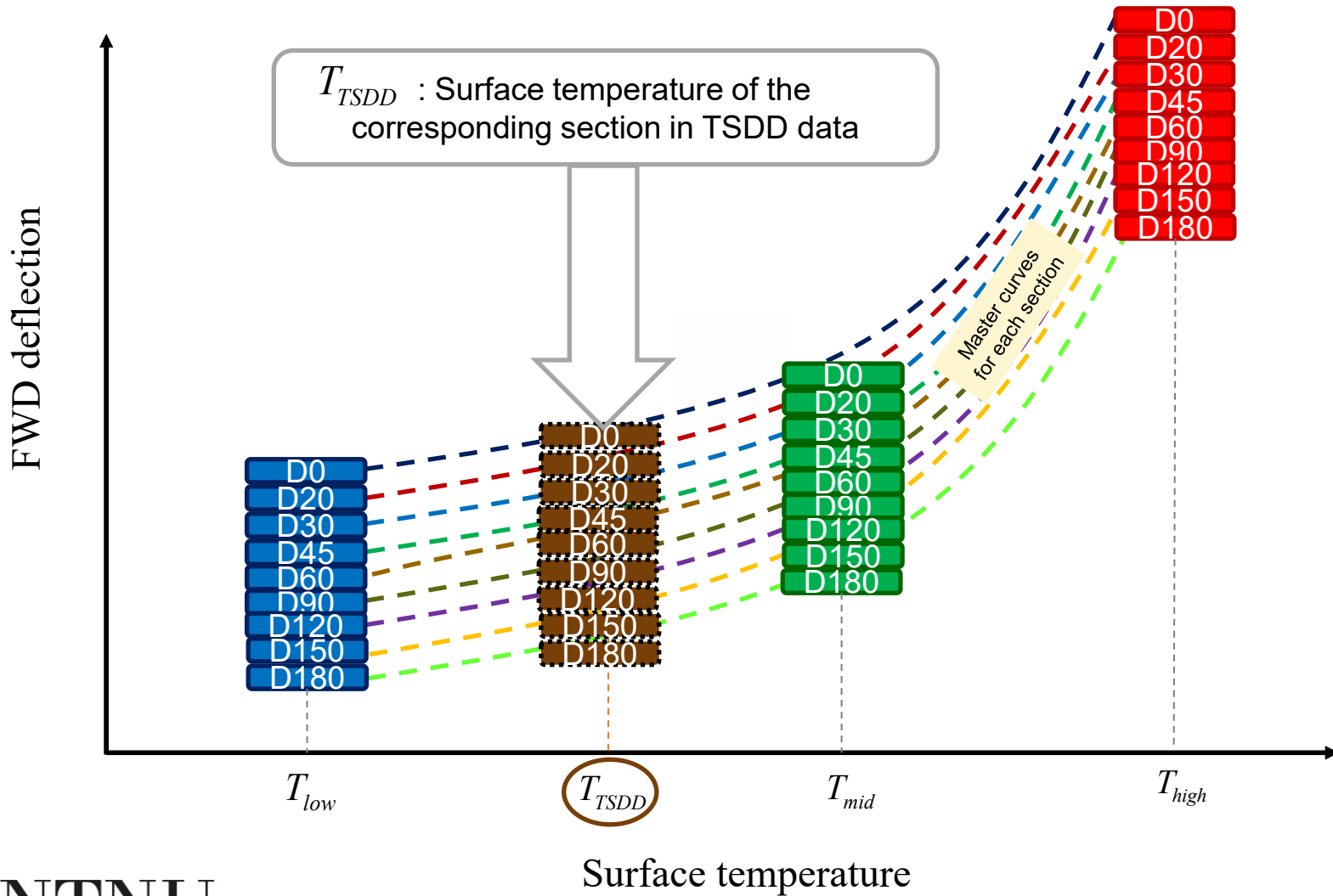
# Location of road sections



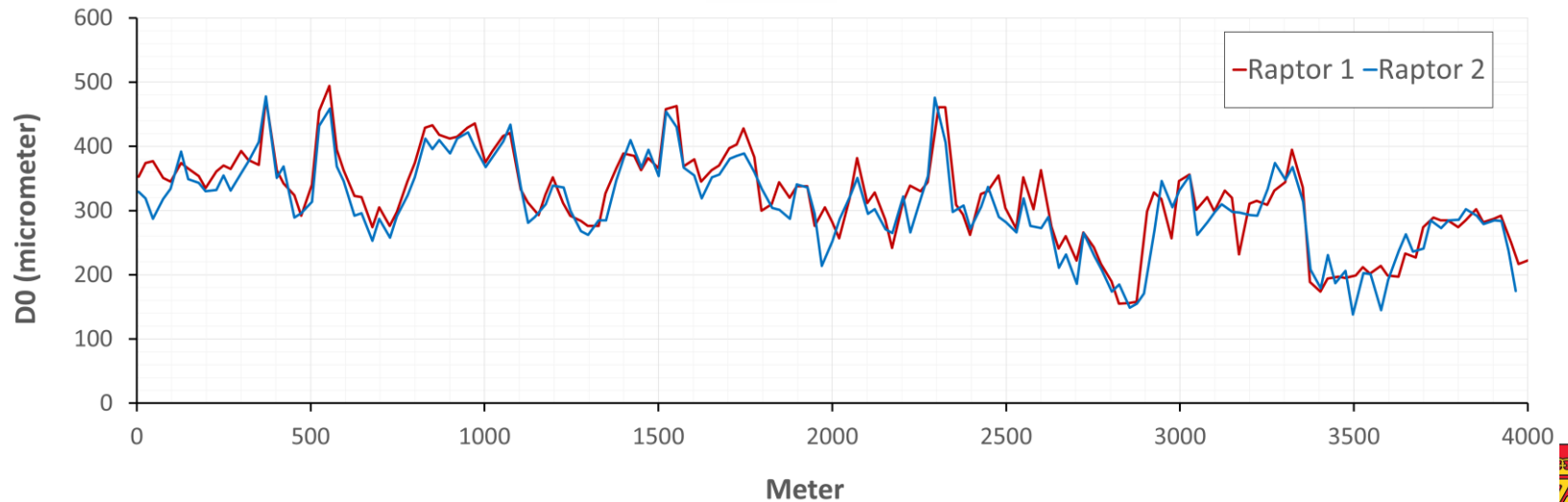
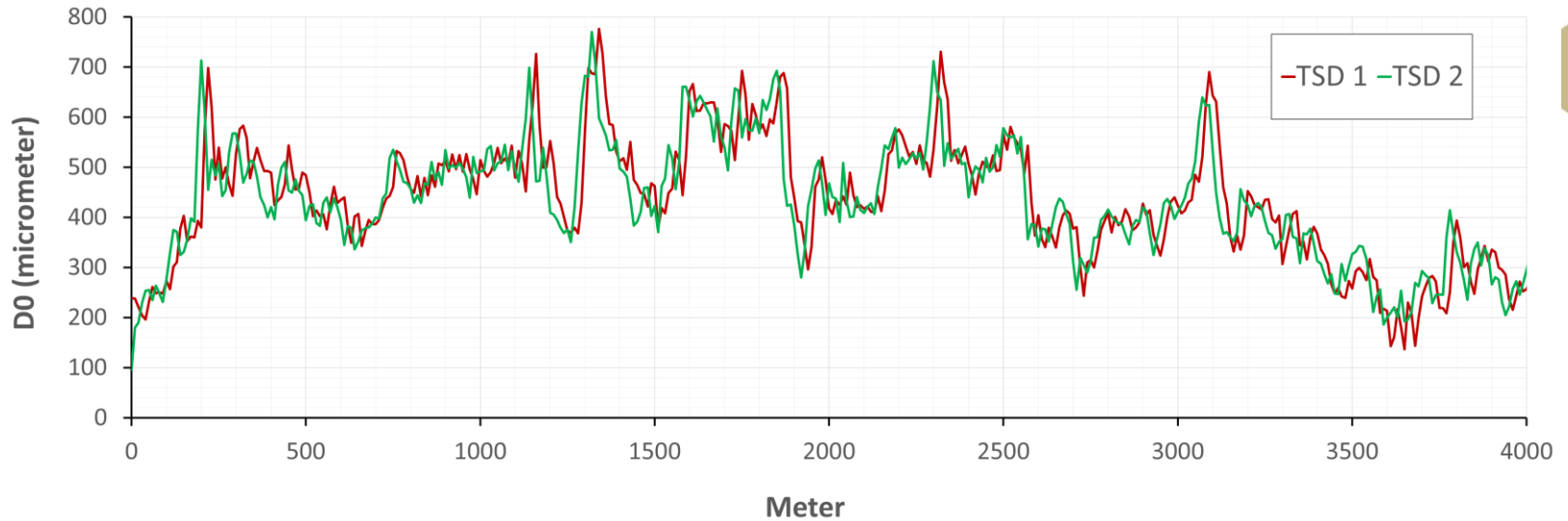
Dataset	Name	Location	Lane	FWD	Raptor	TSD	GPR
1	EV14 S2D1	Stjørdal-Hofstad	Right	✓	✓ ✓	✓ ✓	✓
2	FV705 S1D1	Hell-Leira	Right	✓	✓ ✓	✓	✓
3	EV14 S3D1	Hegramo-Forra	Right	✓	✓ ✓	✓	✓



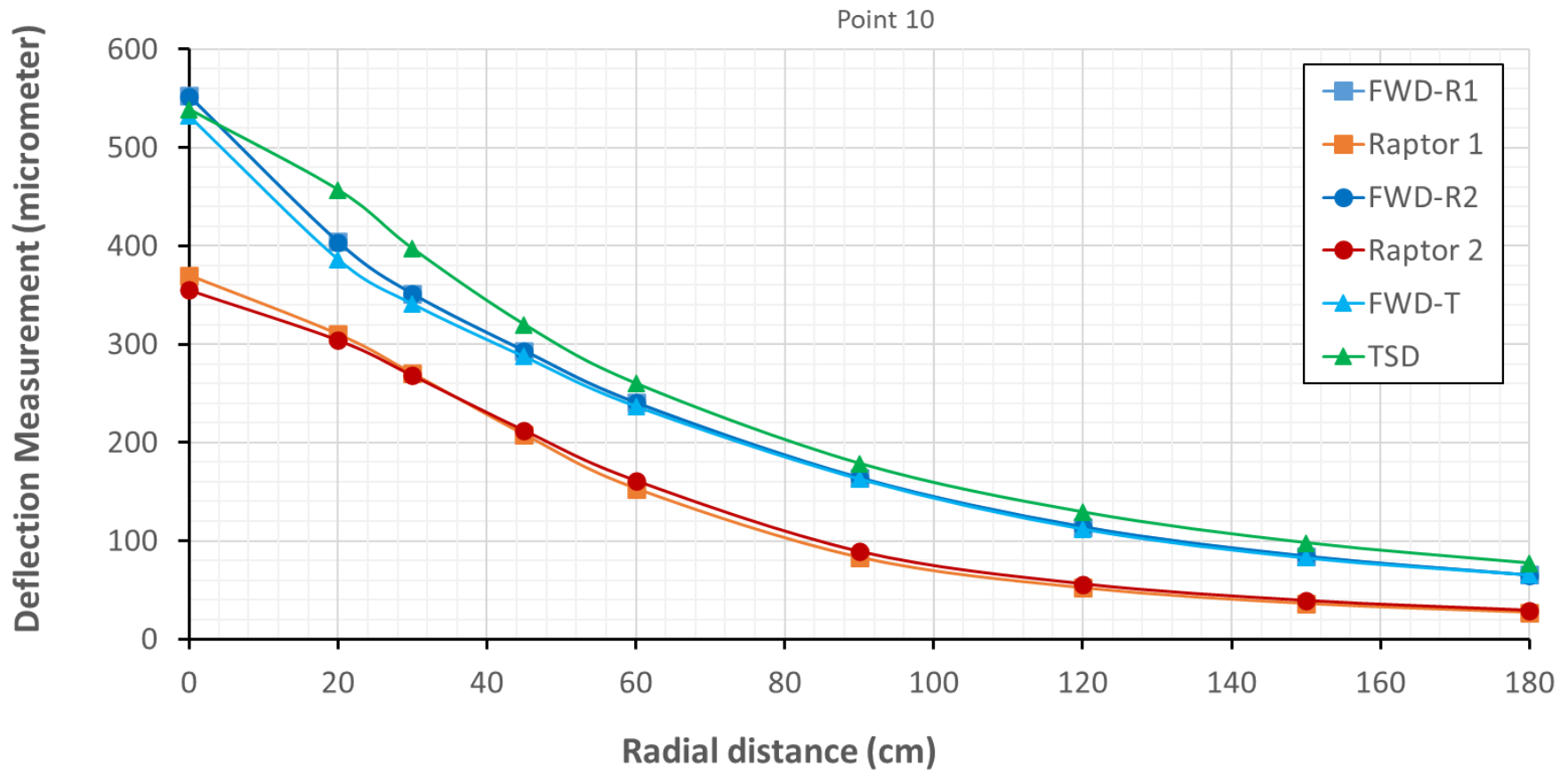
# Temperature effect



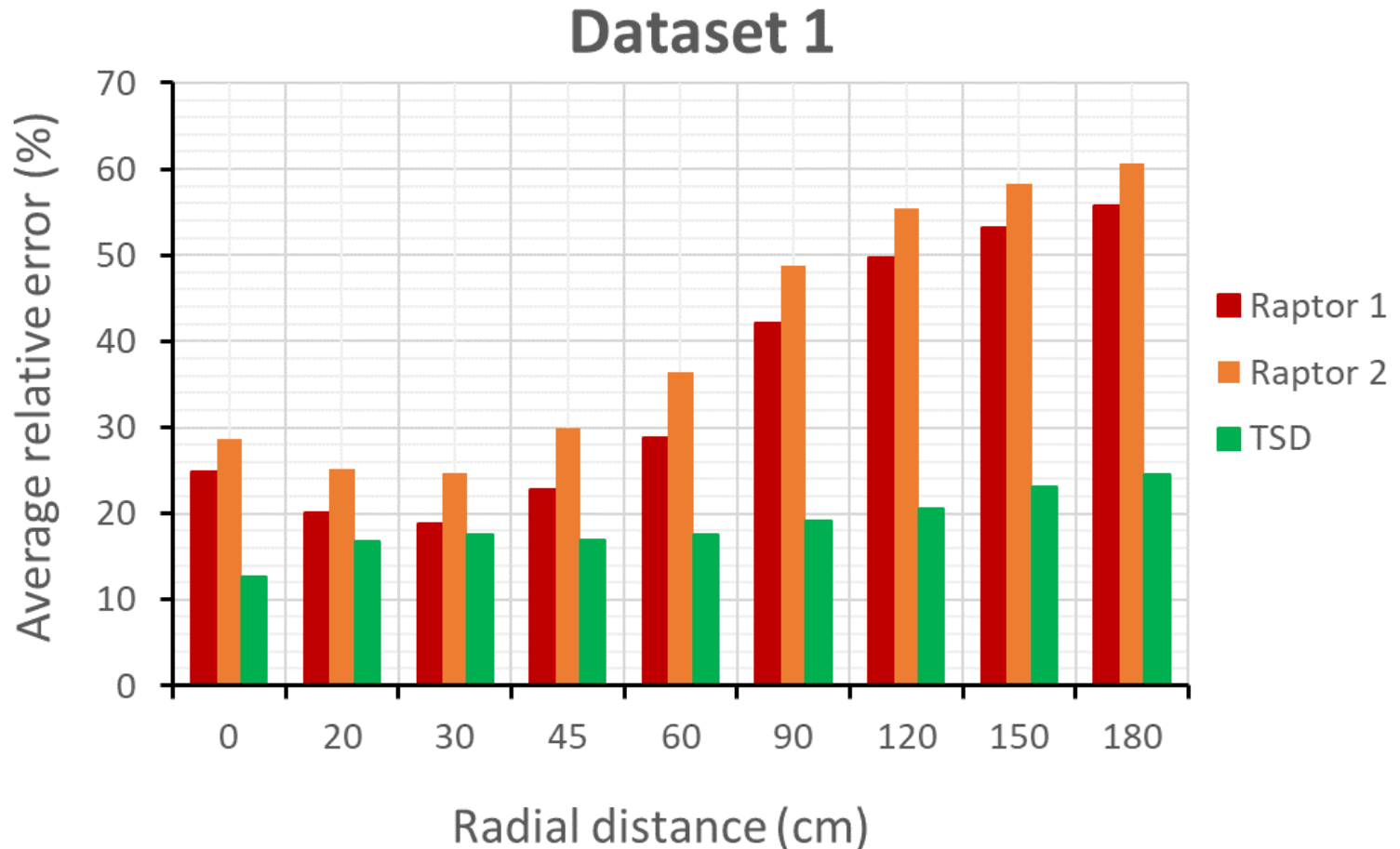
# Repeatability



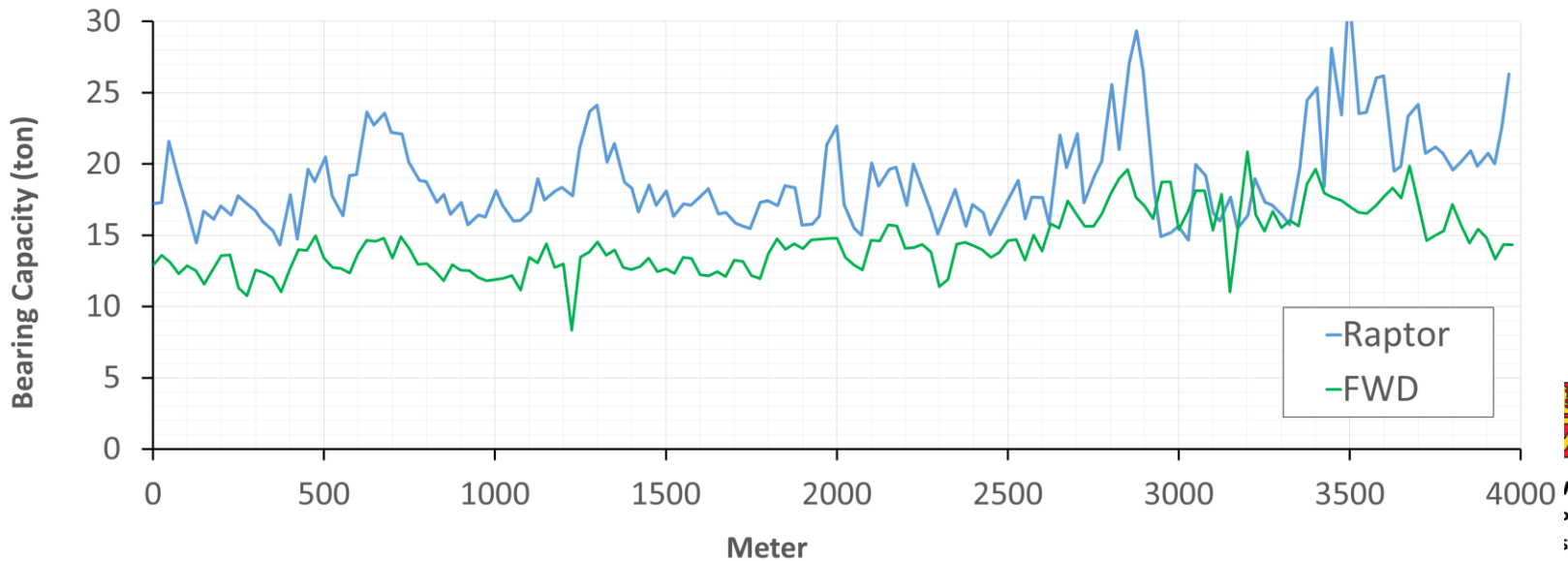
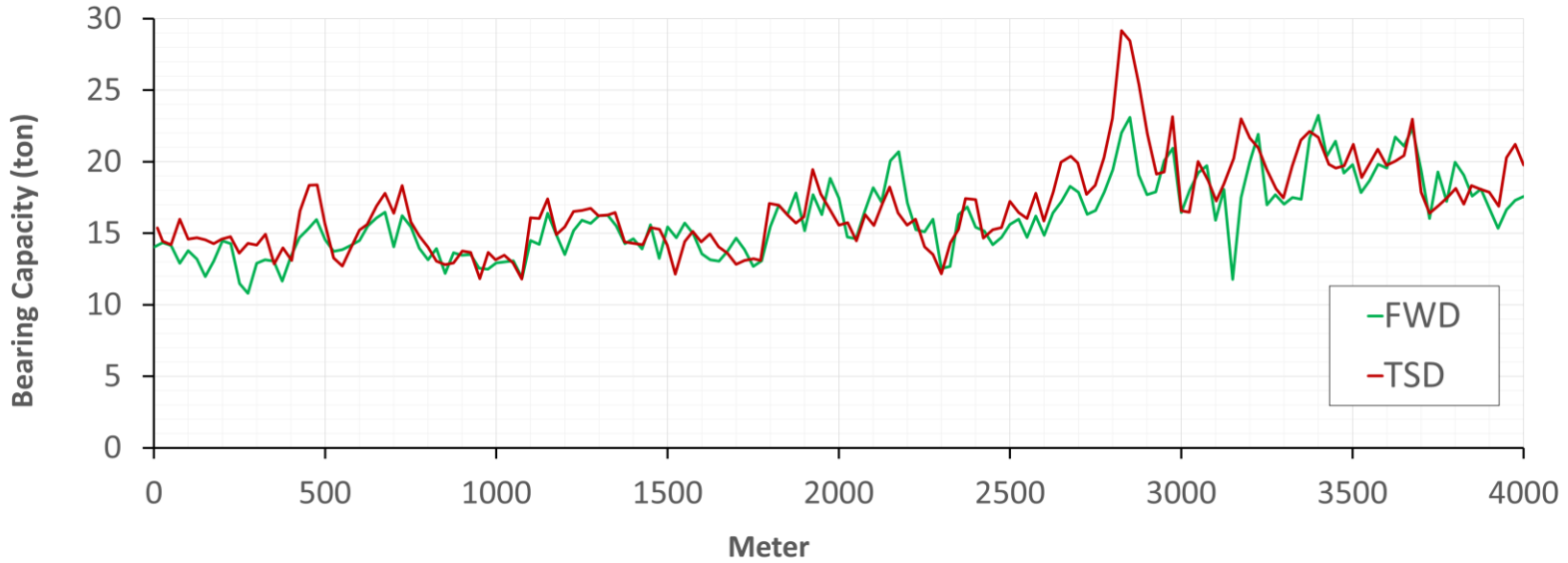
# Graphical comparison



# Statistical comparison

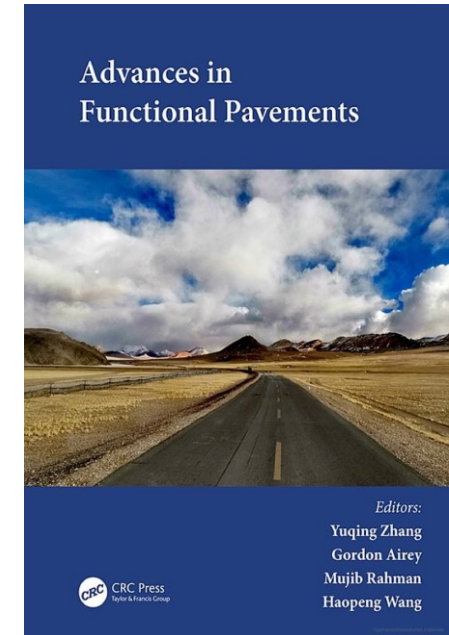


# Structural comparison



# Research papres

- Revising the Norwegian formula for bearing capacity by applying a temperature correction factor
- Consistency between Traffic Speed Deflection Devices and Falling Weight Deflectometer



Taylor & Francis Group  
an informa business

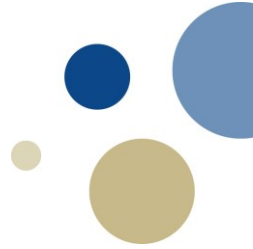


NTNU

Kunnskap for en bedre verden



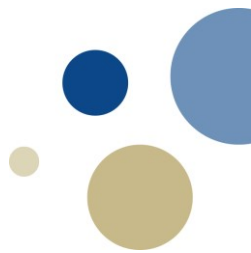
Statens vegvesen  
Norwegian Public Roads  
Administration



# How to use data from TSDDs in the Pavement Management System?

# Obtaining elastic moduli values

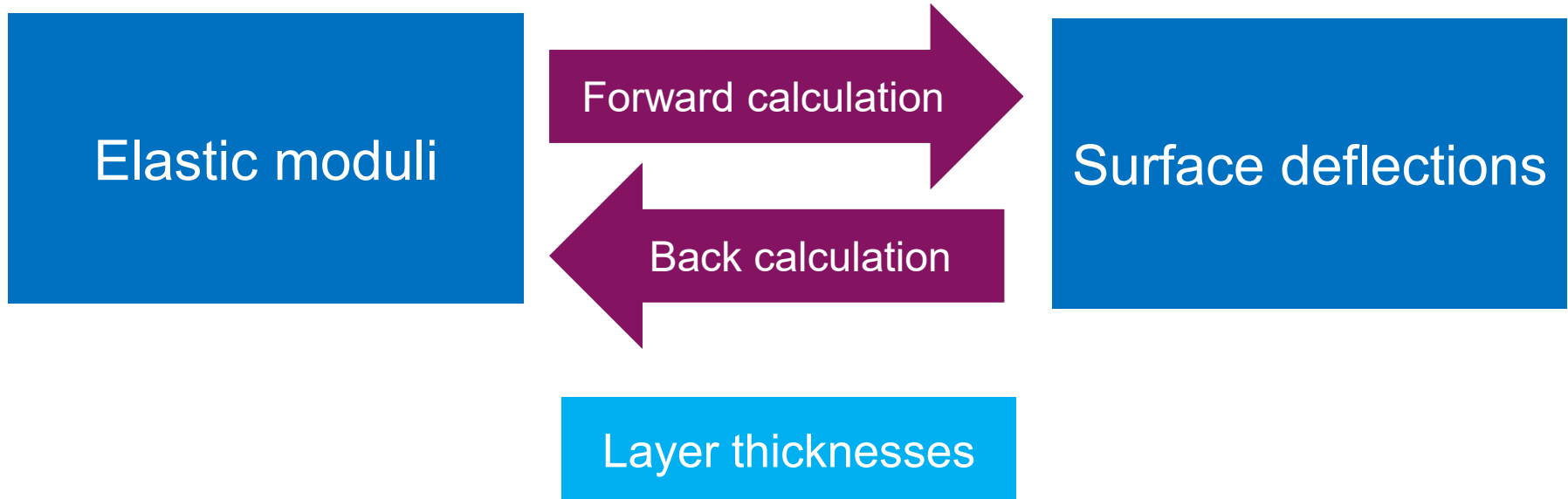
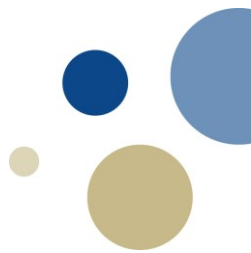
- **Method 1: Directly using elastic back-calculation**
  - ELMOD, BAKFAA, etc. can be used
  - A new elastic back-calculation procedure can be defined
- **Method 2: Correcting data from TSDDs, then using elastic back-calculation**
  - Compare TSDDs deflections with equivalent FWD deflections
  - Develop regression models for each radial distance
  - Use the corrected values in an elastic back-calculation process
- **Method 3: Using viscoelastic back-calculation**
  - Greenwood's back-calculation procedure
  - Potential of defining a new viscoelastic back-calculation software



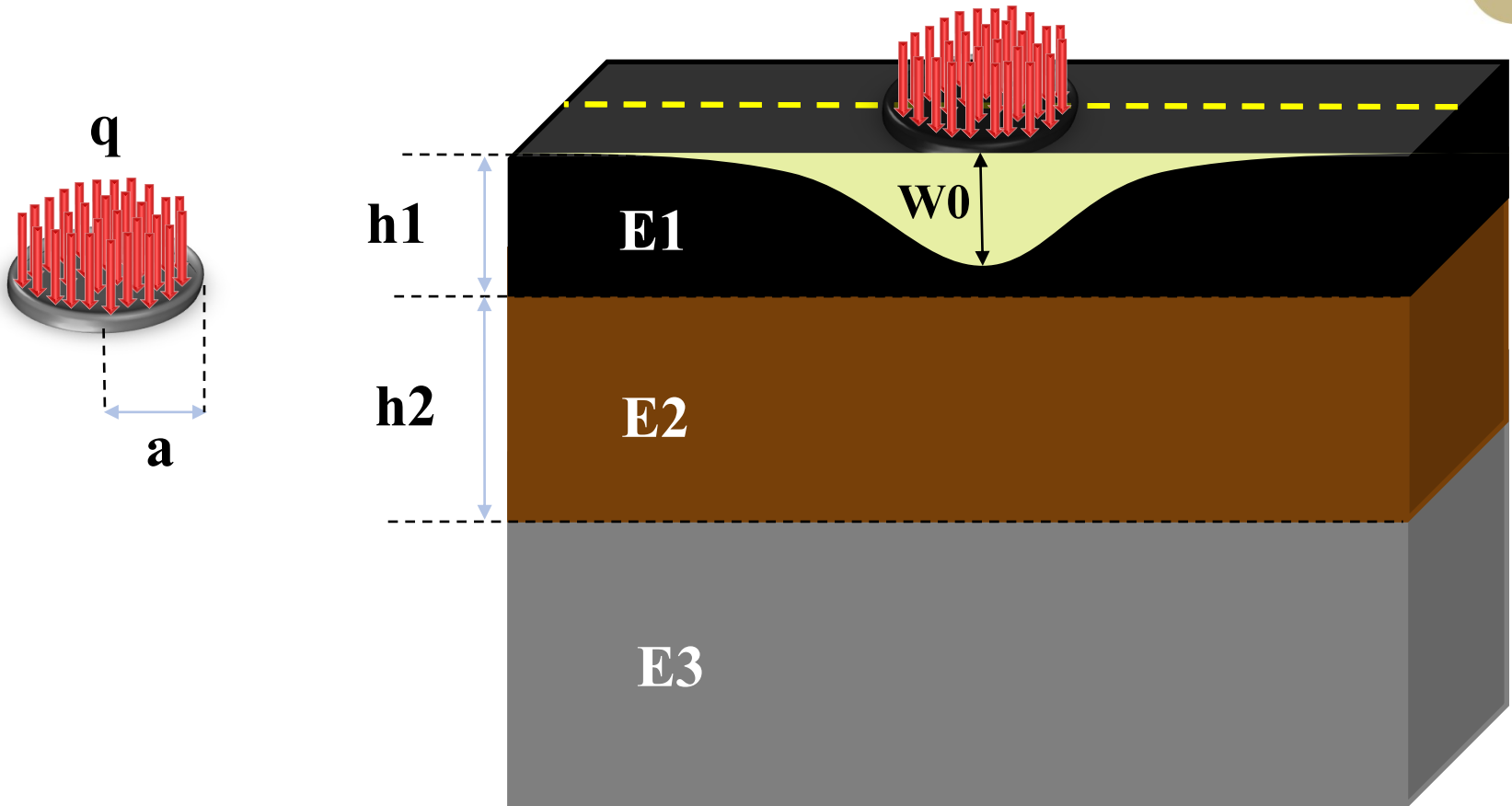


# Forward- and back-calculation

- Deflections: Forward calculation
- Elastic moduli: Back calculation

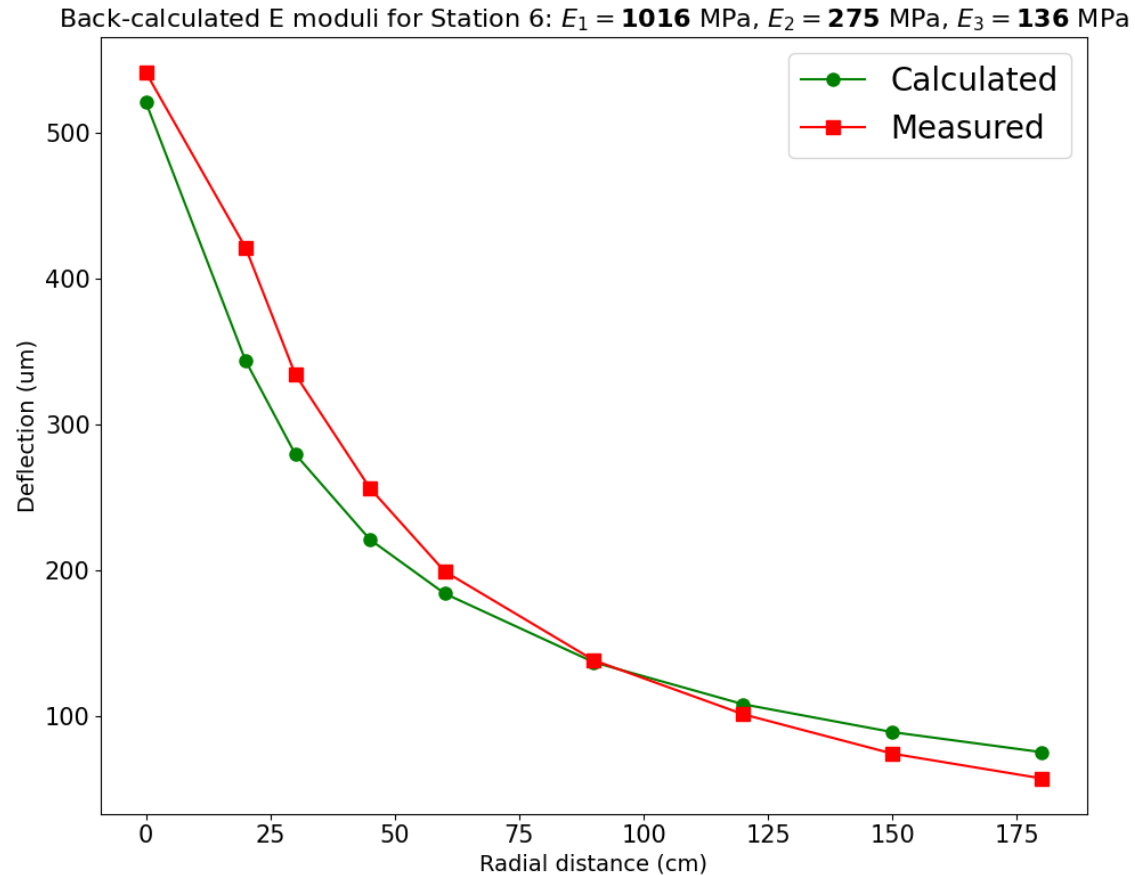


# Pavement structure: A 3-layer system

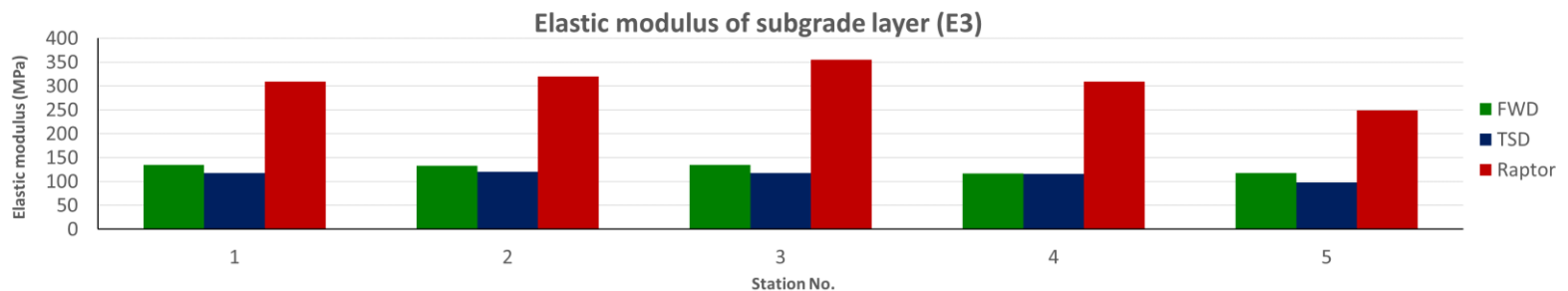
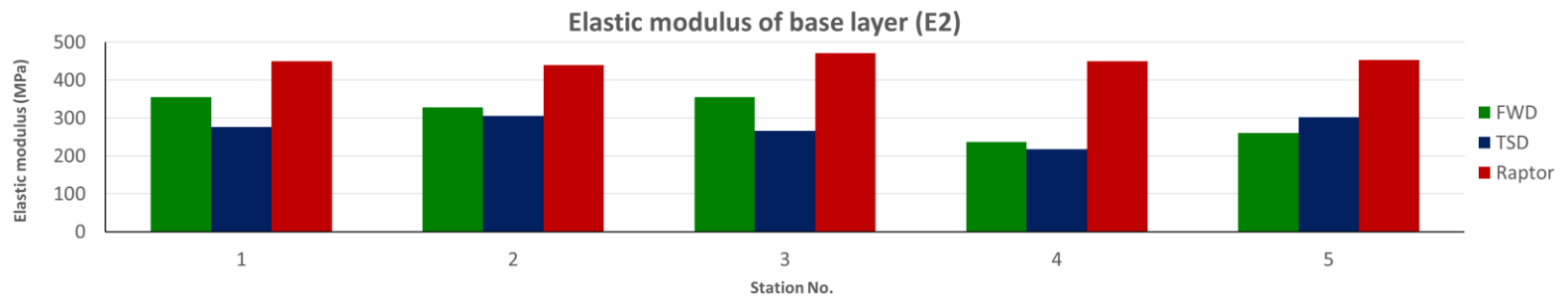
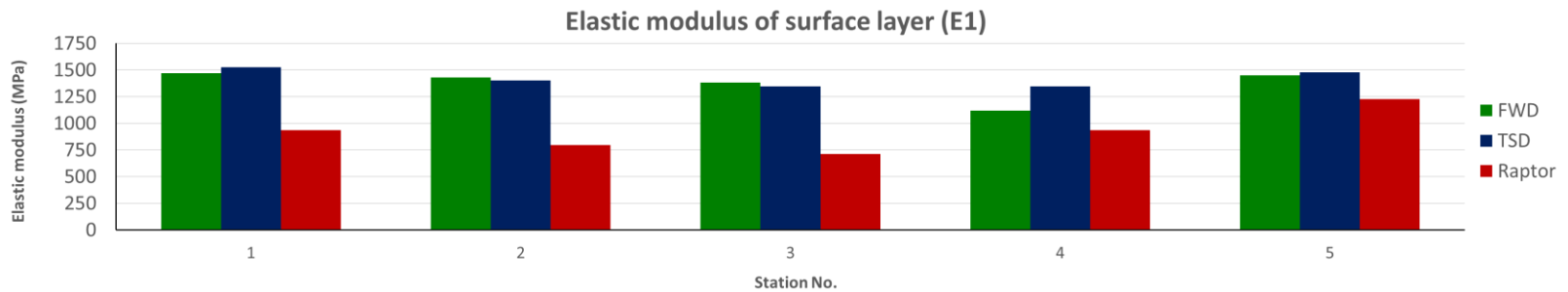


# Elastic back-calculation

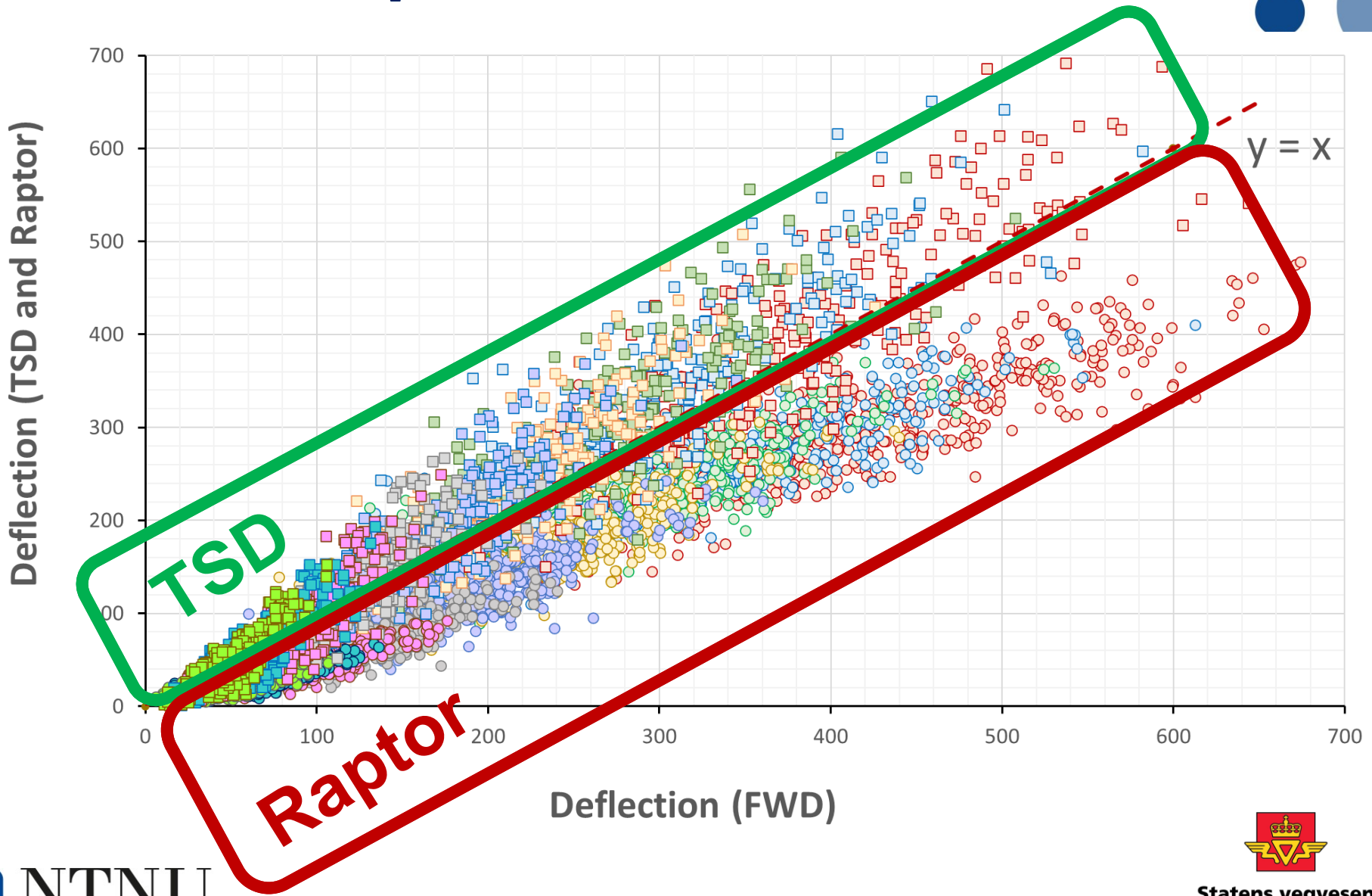
- A new back-calculation computer program



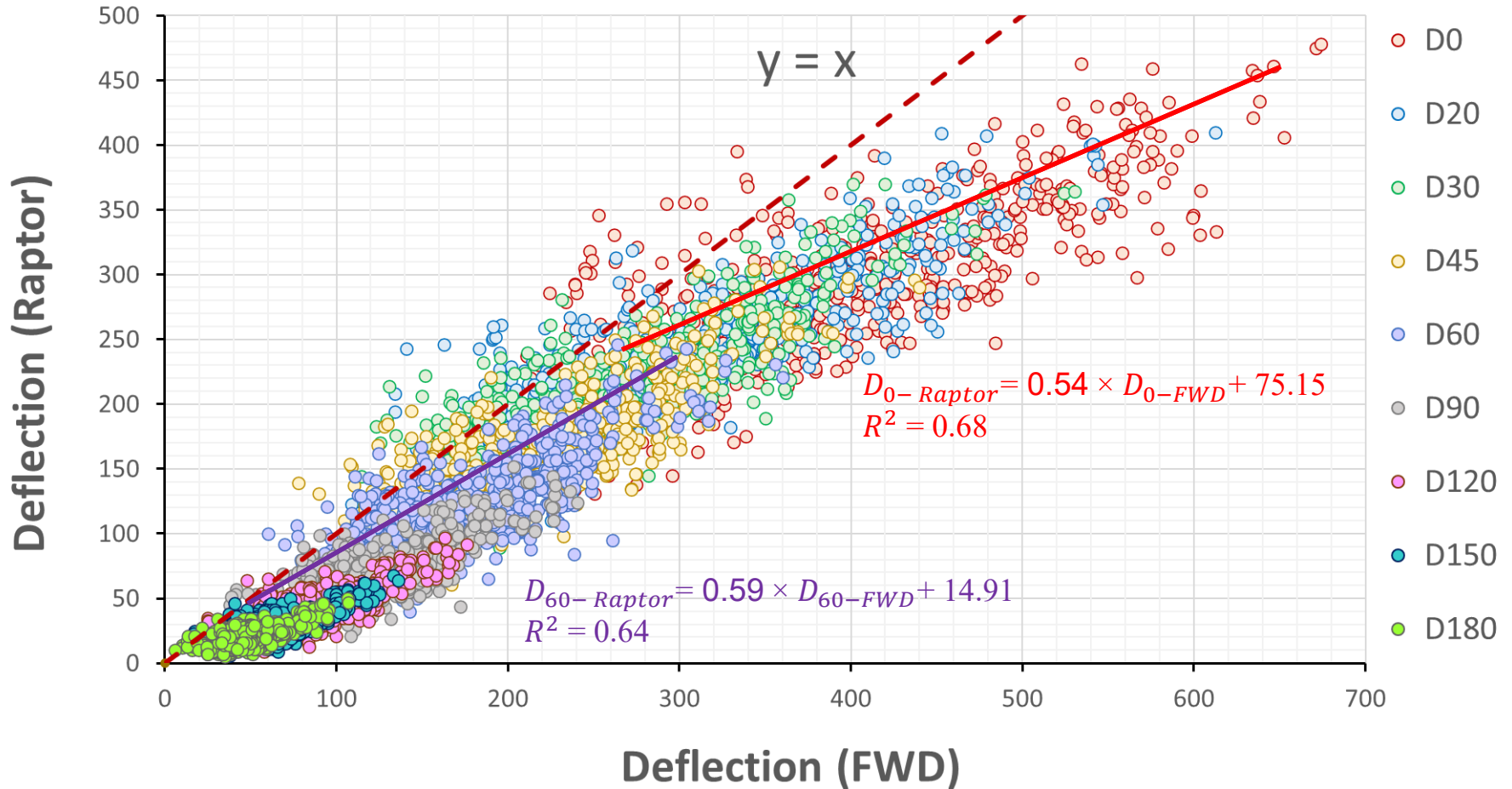
# Method 1: Elastic moduli (without correction)



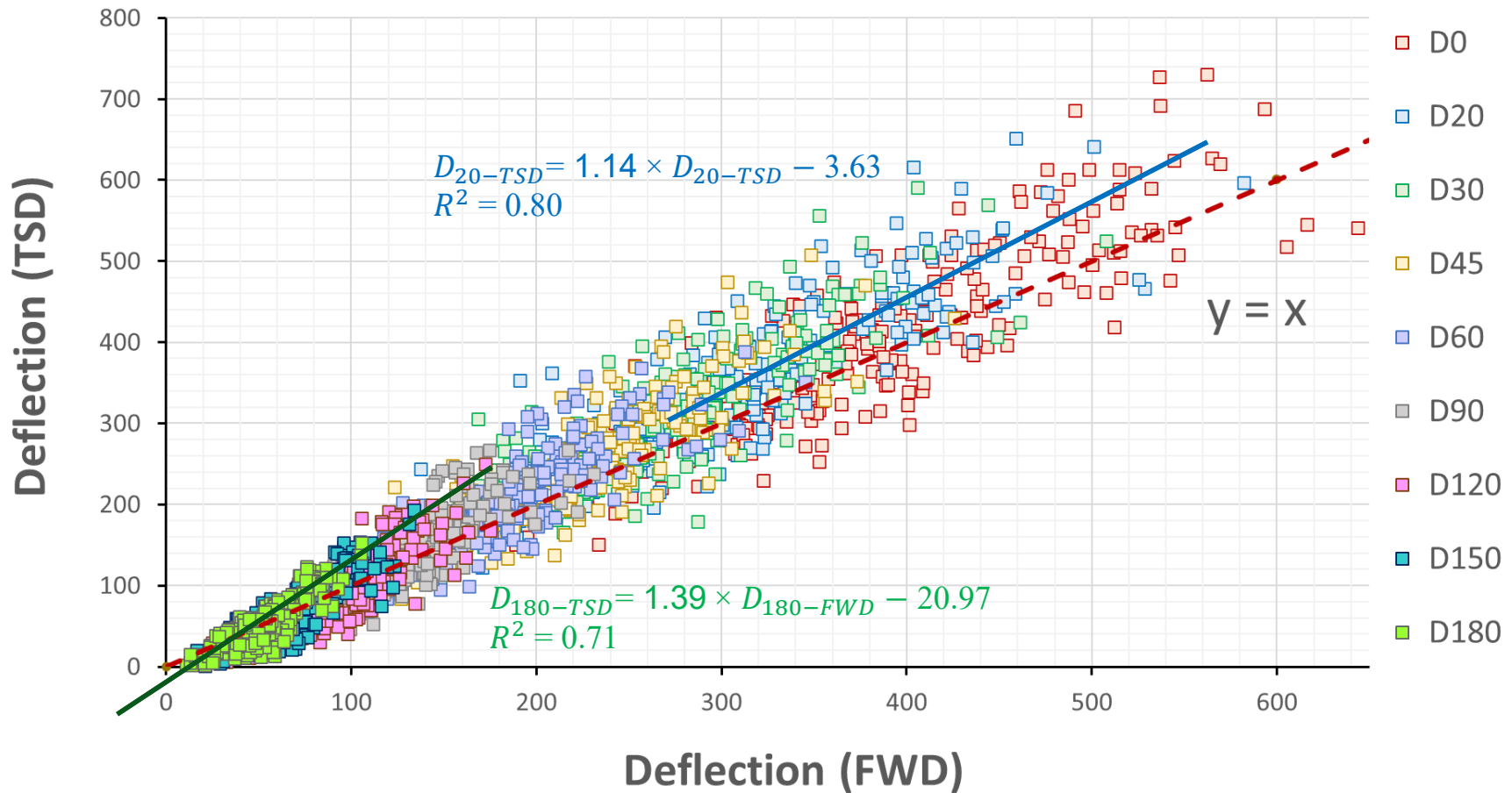
# TSD and Raptor versus FWD



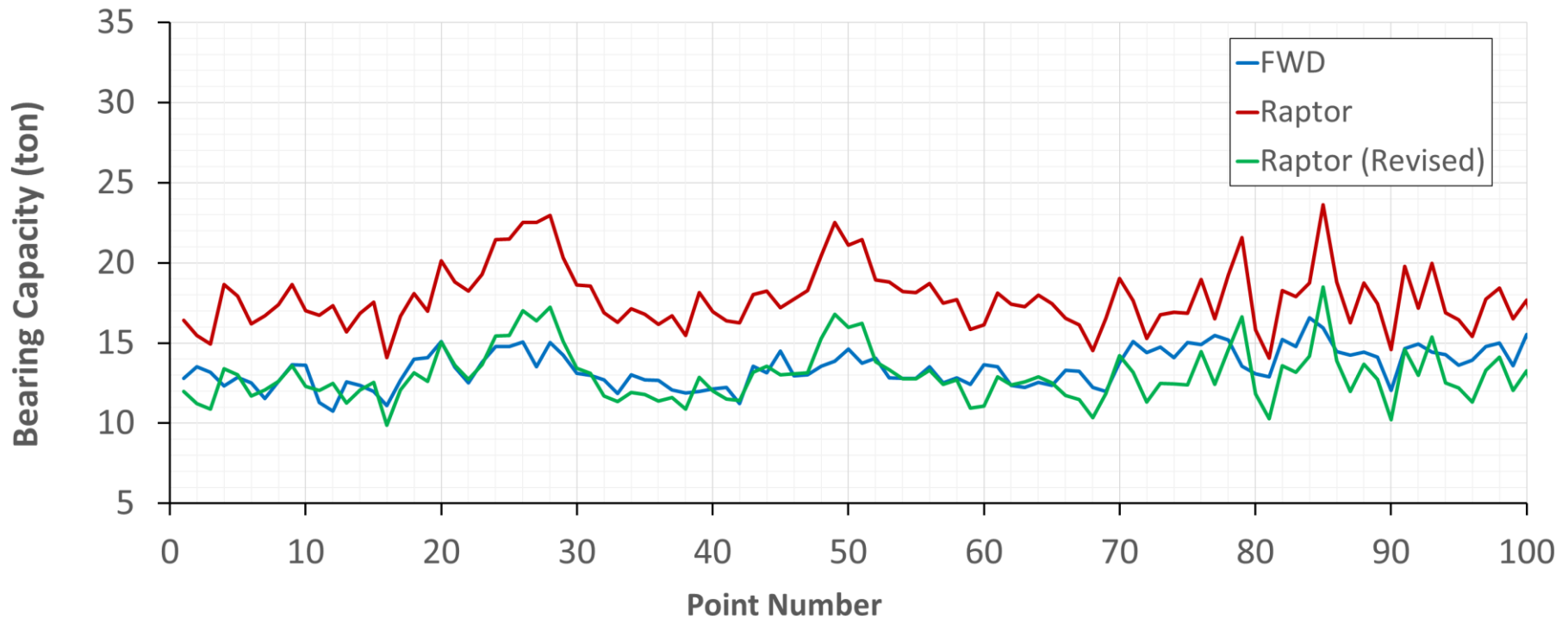
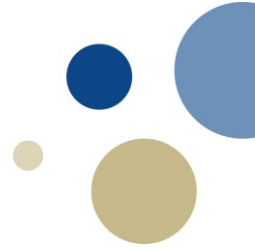
# Raptor and FWD



# TSD and FWD

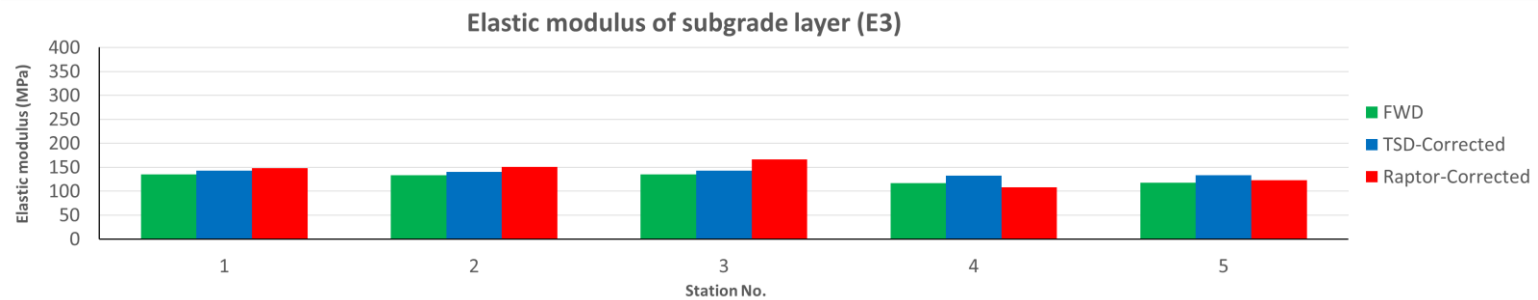
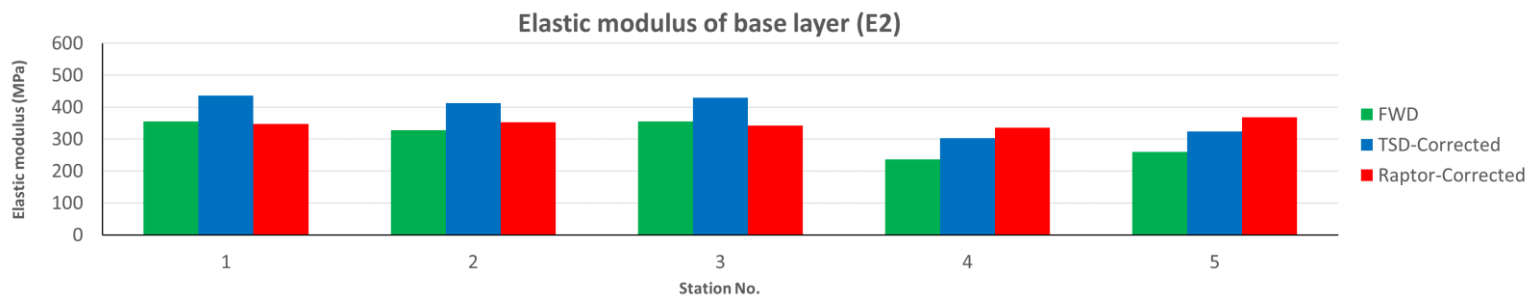
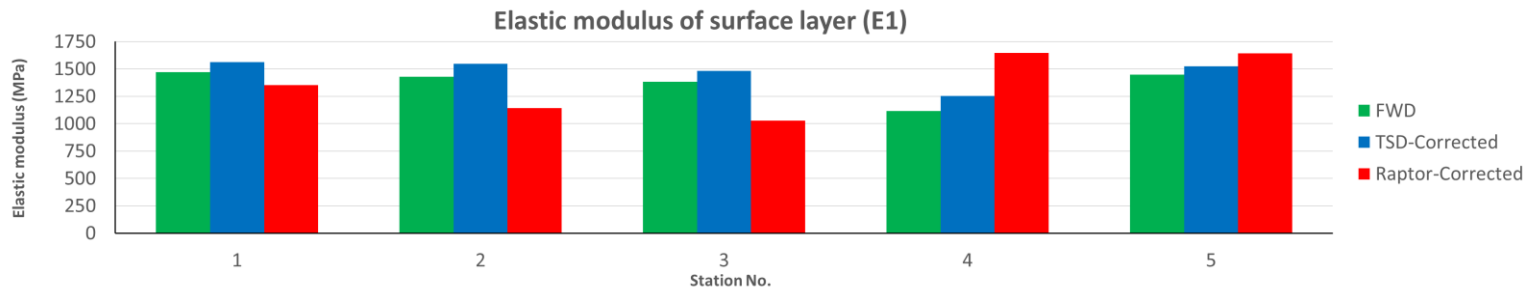


# Bearing capacity after refinement





# Method 2: Elastic moduli (after correction)



# Elastic back-calculation: Challenges

- Asphalt layers are viscoelastic and not elastic
- Regression models between TSDDs and FWD can differ from road to road
- The effect of moving load is not reflected
- Driving speed might have effect on deflections
- Temperature difference is not reflected
- Mixture type might affect deflections
- Design frequency in dynamic modulus master curves

Viscoelastic Analysis

# Viscoelastic characteristics

- Elastic behavior
- Viscoelastic behavior
  - Dynamic modulus test

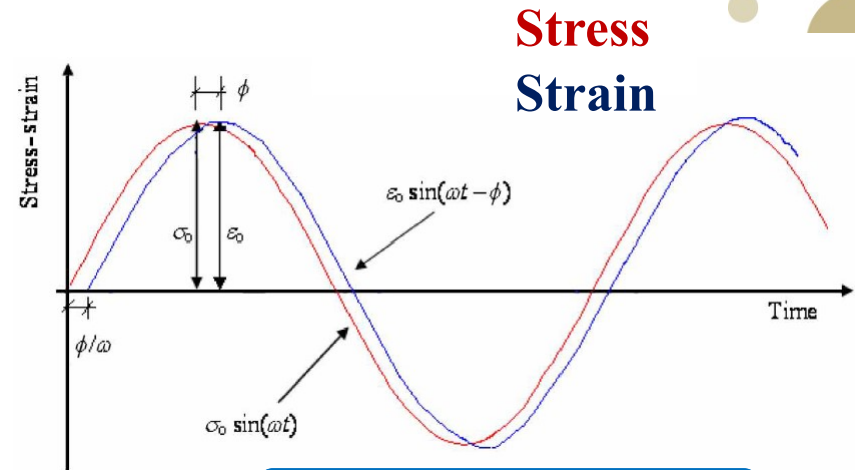
$$E^* = E' + iE''$$

$E^*$  : Complex modulus

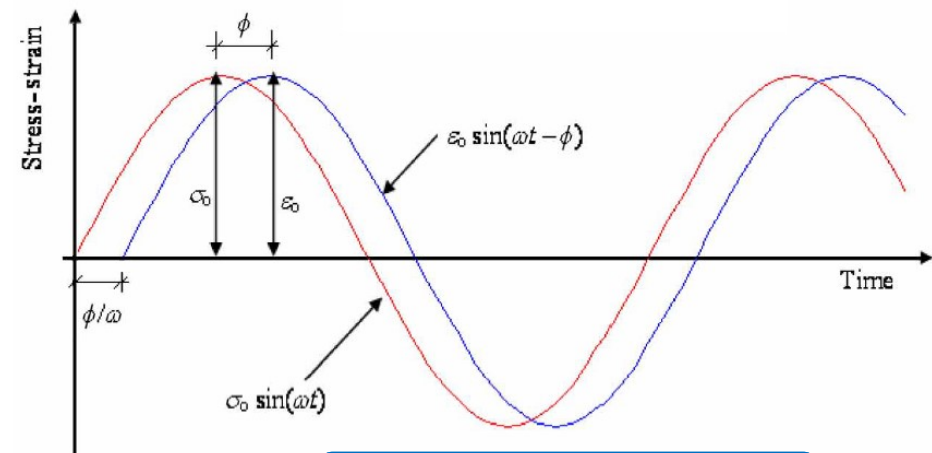
$E'$  : Storage modulus

$E''$  : Loss modulus

$|E^*|$  : Dynamic modulus



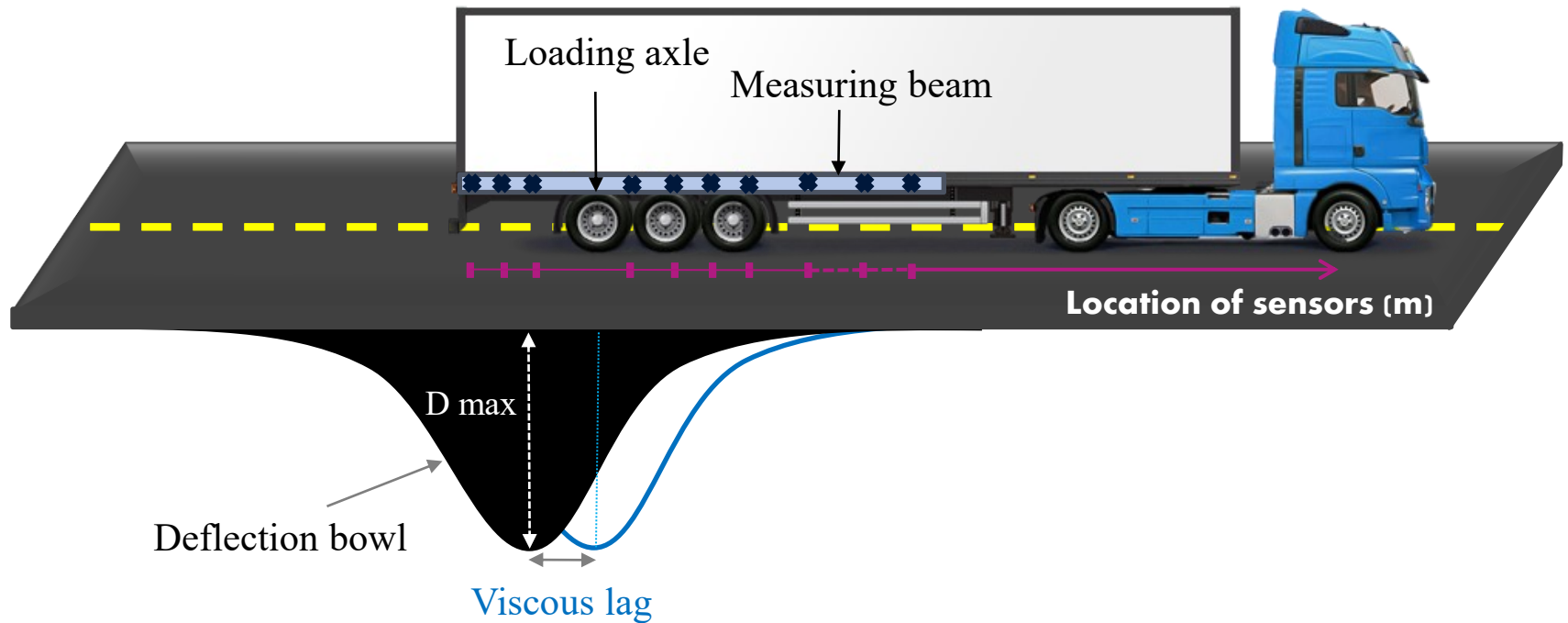
Elastic material



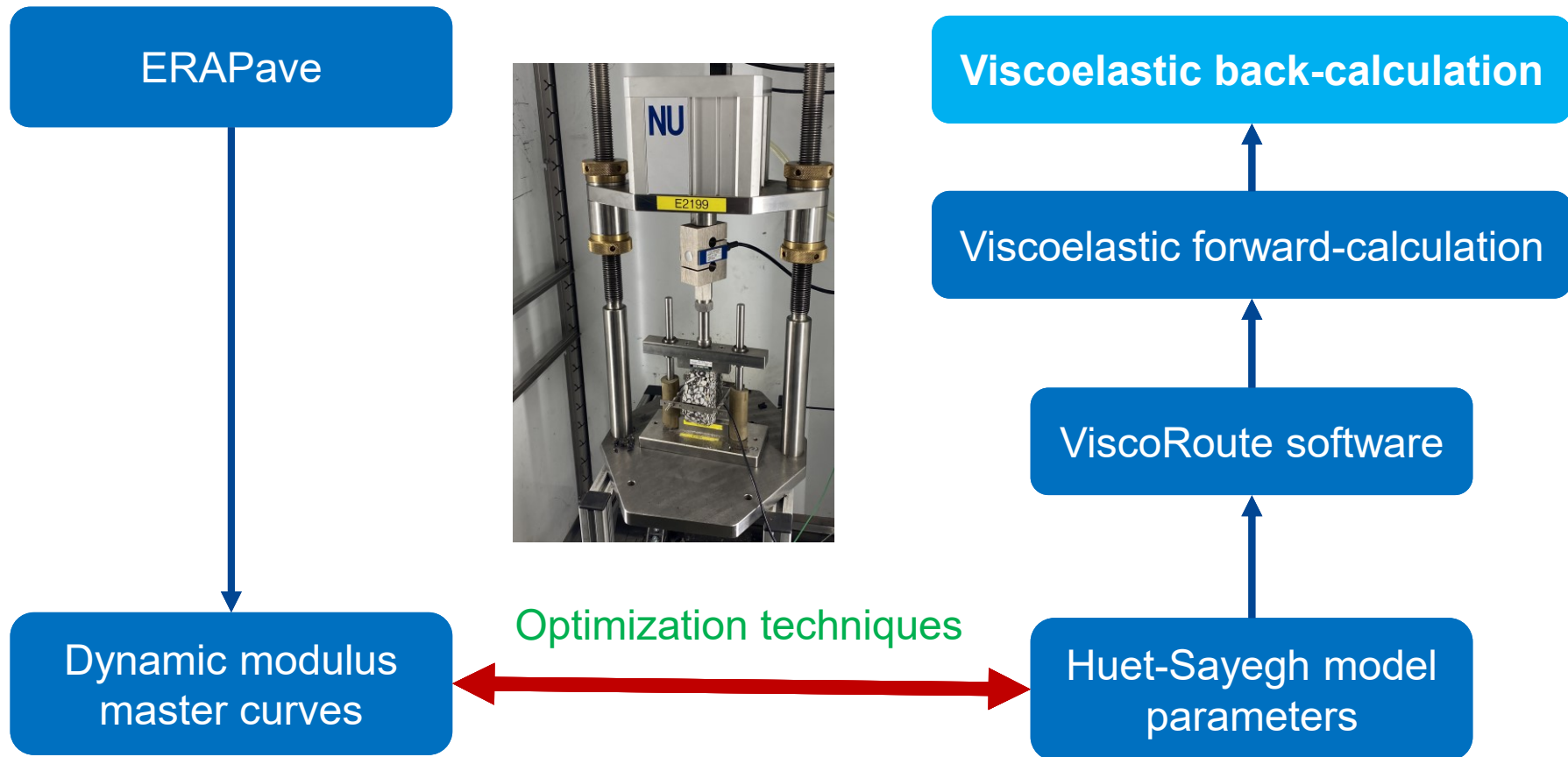
Viscoelastic material

# TSD: Viscous lag

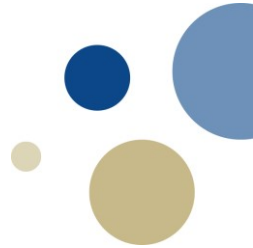
- Three sensors are behind the TSD's loading axle
- A lag distance can be detected



# Considering viscoelasticity



# Dynamic modulus test



$$E^* = |E^*| \cos \varphi + i |E^*| \sin \varphi$$

$$\log(|E^*|) = a + \frac{b}{1 + e^{c-d[\log(f_r)]}}$$

$$\log(a_T) = \frac{-C_1(T - T_r)}{C_2 + (T - T_r)}$$

$$\log(f_r) = \log(a_T) + \log(f)$$

$$\varphi = \frac{k_p \cdot k_g^2}{[\log(f_r) - k_c]^2 + k_g^2}$$

$$\Rightarrow |E^*| = 10 \left( a + \frac{b}{1 + e^{c-d \left( \frac{-C_1(T - T_r)}{C_2 + (T - T_r)} + \log(f) \right)}} \right)$$

# Huet-Sayegh model

$$E^* = E_0 + \frac{E_\infty - E_0}{1 + \delta [i\omega\tau(\theta)]^{-k} + [i\omega\tau(\theta)]^{-h}}$$

$$\tau(\theta) = \exp(A_0 + A_1\theta + A_2\theta^2)$$

$$M = \frac{1 + \delta [\omega\tau(\theta)]^{-k} \cos \frac{\pi k}{2} + [\omega\tau(\theta)]^{-h} \cos \frac{\pi h}{2}}{E_\infty - E_0}$$

$$N = \frac{\delta [\omega\tau(\theta)]^{-k} \sin \frac{\pi k}{2} + [\omega\tau(\theta)]^{-h} \sin \frac{\pi h}{2}}{E_\infty - E_0}$$

$$E^* = E' + iE'' = \left( E_0 + \frac{M}{M^2 + N^2} \right) + i \cdot \frac{N}{M^2 + N^2}$$

$$\Rightarrow |E^*| = \sqrt{\left( E_0 + \frac{M}{M^2 + N^2} \right)^2 + \left( \frac{N}{M^2 + N^2} \right)^2}$$

# Finding model parameters

- Equate the two models:

- Loss modulus  $|E^*| \cos \varphi = E_0 + \frac{M}{M^2 + N^2}$

- Storage modulus  $|E^*| \sin \varphi = \frac{N}{M^2 + N^2}$

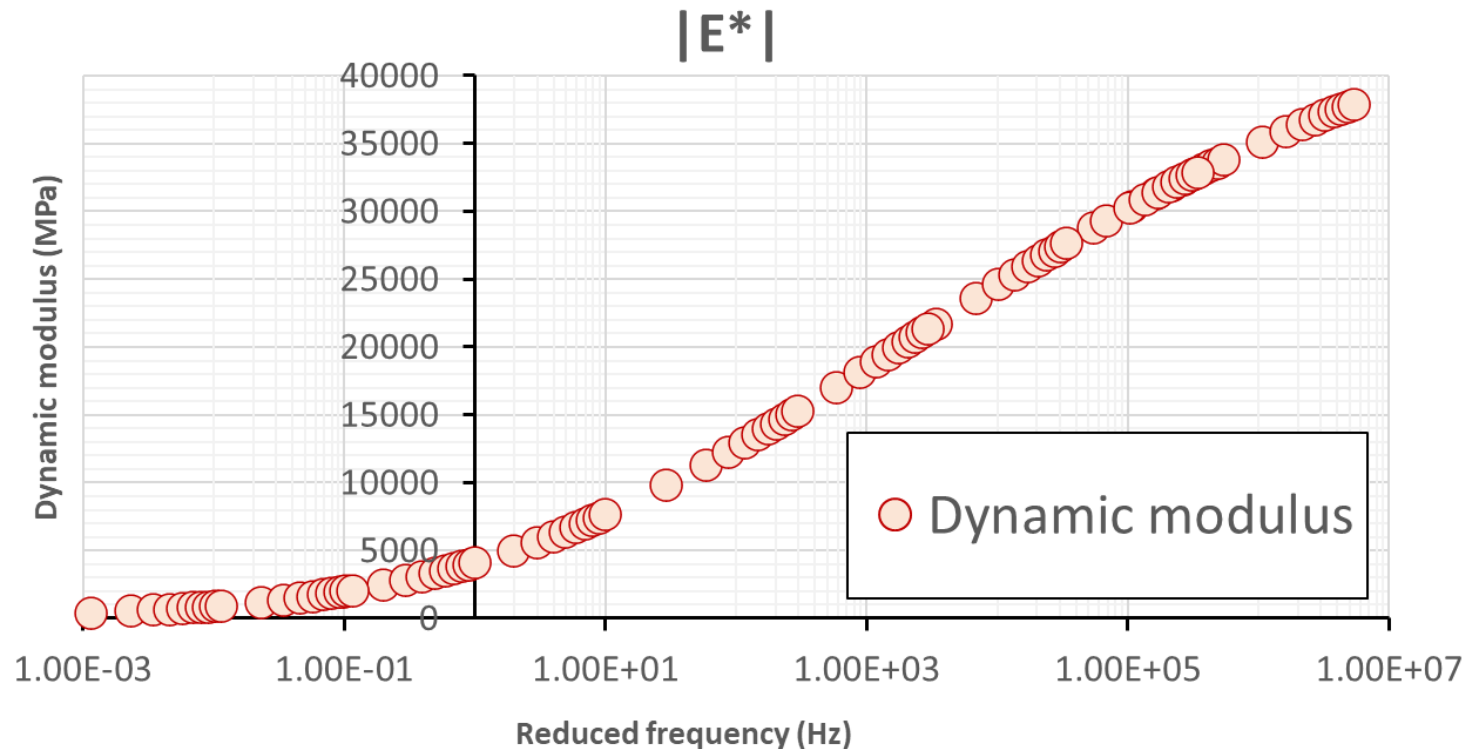
- Dynamic modulus

$$10 \left( a + \frac{b}{1 + e^{\frac{c-d \left( \frac{-C_1(T-T_r)}{C_2+(T-T_r)} + \log(f) \right)}{}} \right) = \sqrt{\left( E_0 + \frac{M}{M^2 + N^2} \right)^2 + \left( \frac{N}{M^2 + N^2} \right)^2}$$



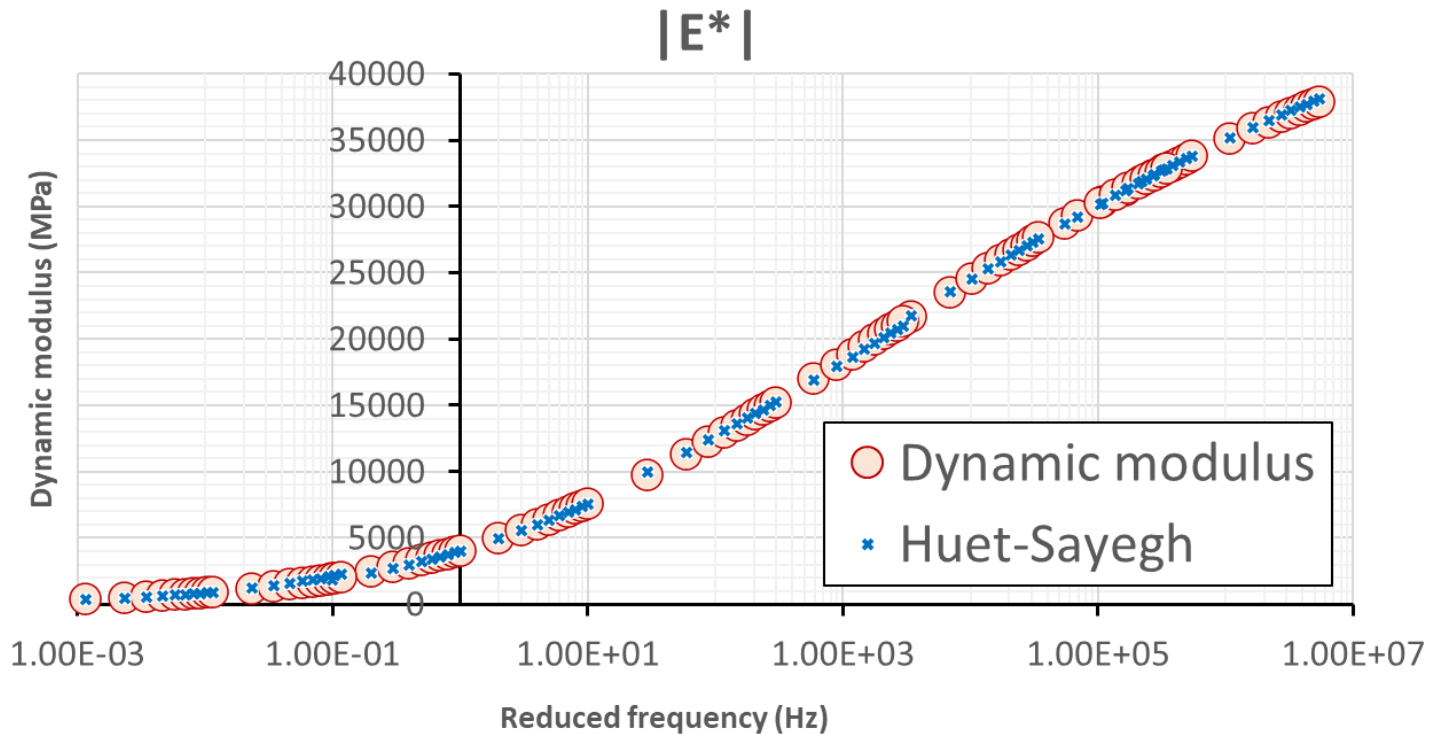
# Dynamic modulus model parameters

- For each mixture type, dynamic modulus model parameters ( $a$ ,  $b$ ,  $c$ ,  $d$ ,  $C1$ ,  $C2$ ,  $k_p$ ,  $k_g$ ,  $k_c$ ) are known



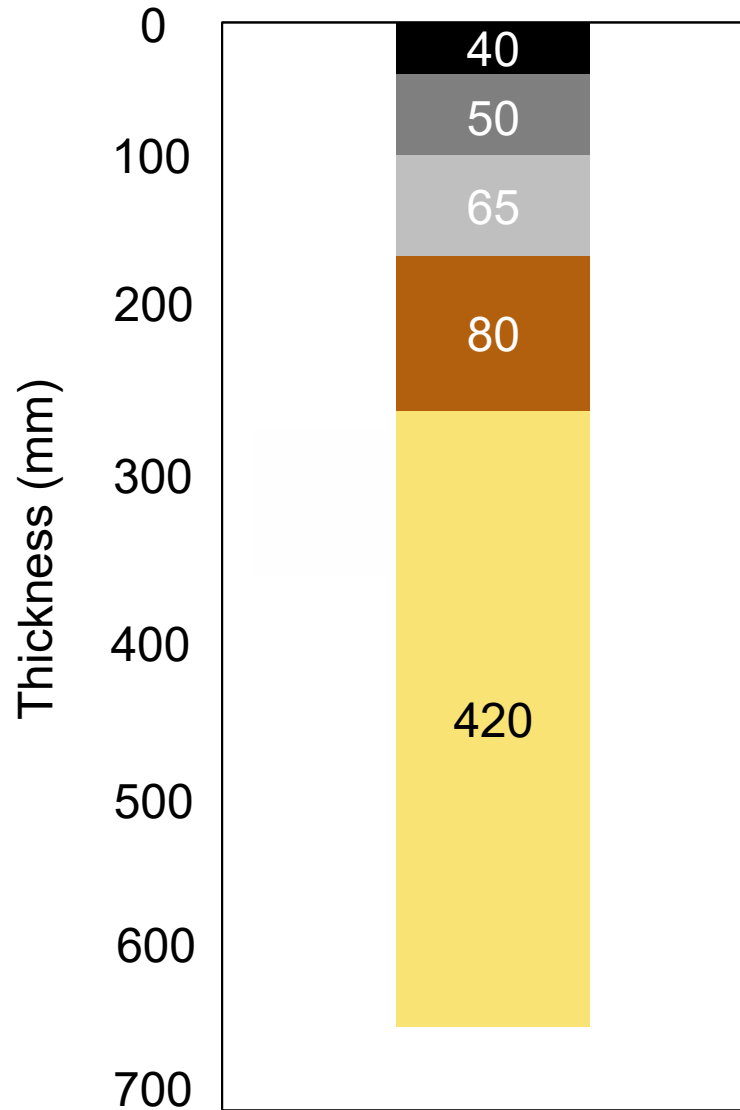
# Huet-Sayegh model parameters

- For the same mixture, corresponding Huet-Sayegh model parameters ( $k$ ,  $h$ ,  $\delta$ ,  $A_0$ ,  $A_1$ ,  $A_2$ ,  $E_0$ ,  $E_s$ ) are obtained using optimization techniques



# A sample structure in ERAPave

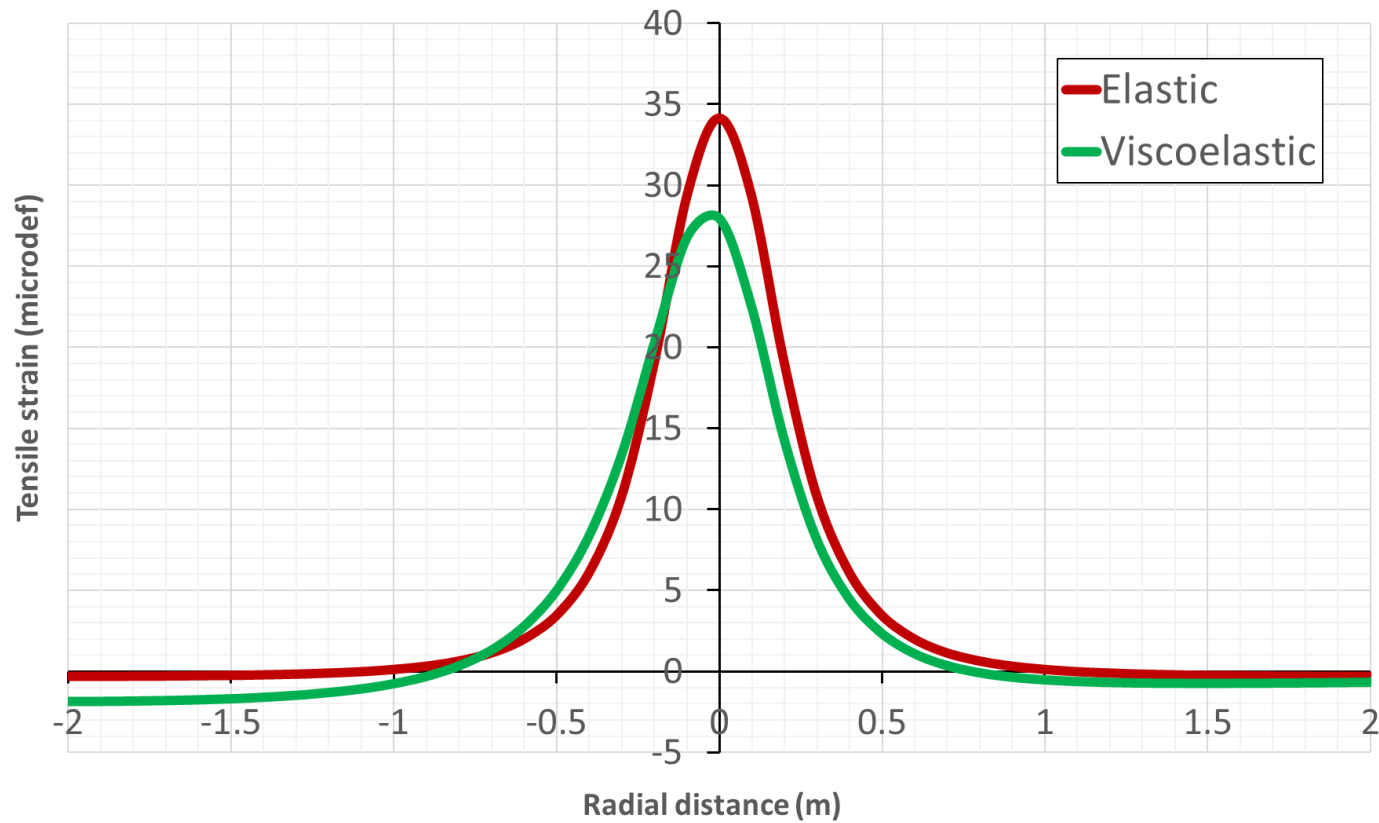
- A sample structure
- Layer properties
  - SMA 11-70/100
  - AC 16-70/100
  - AC 16-160/220
  - Knust berg
  - Knust berg
  - Silt,  $cu < 25$



- Surface layer
- Bituminous binder layer
- Bituminous base layer
- Unbound base layer
- Subbase layer

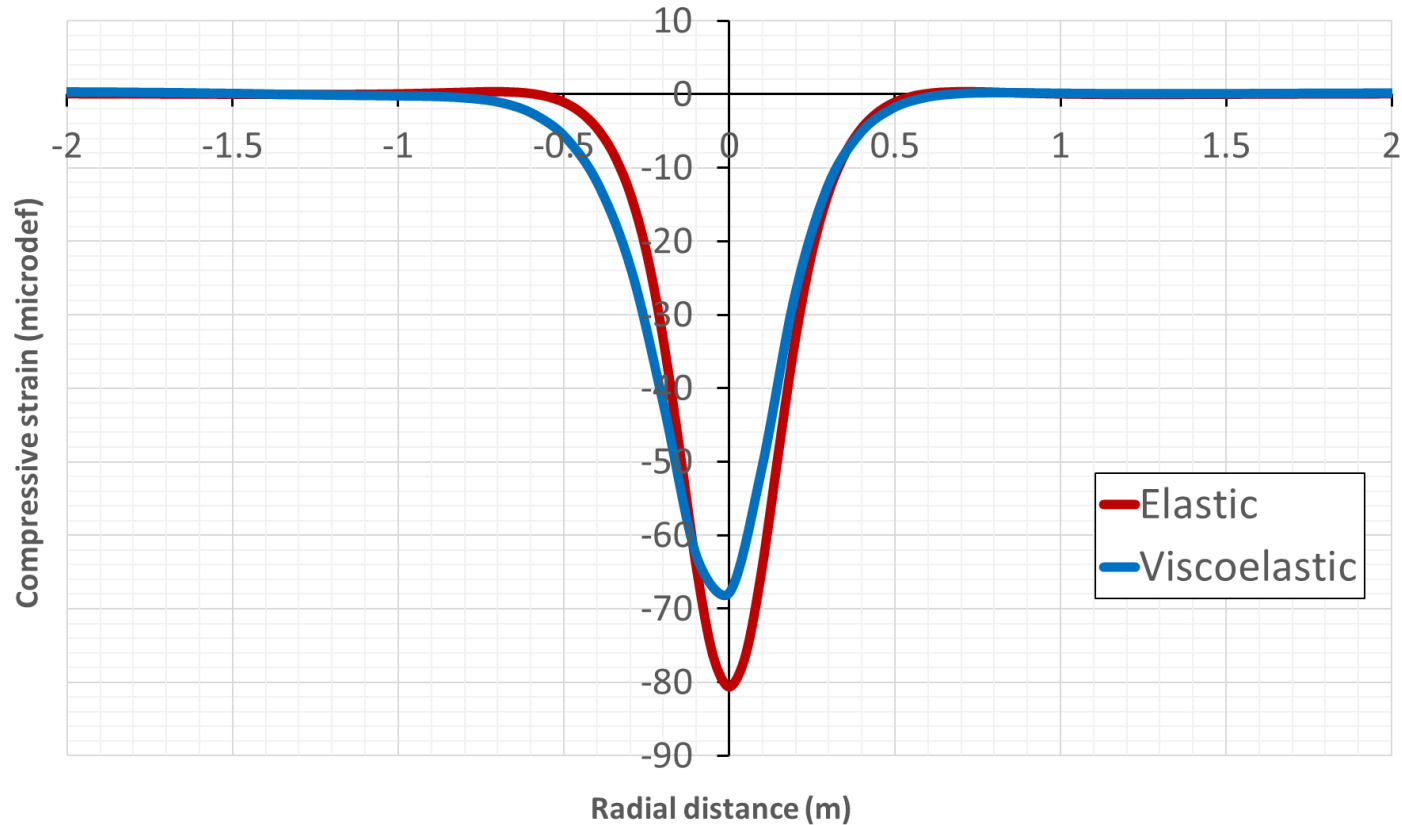
# Fatigue model

- Tensile strain at the bottom of asphalt layers

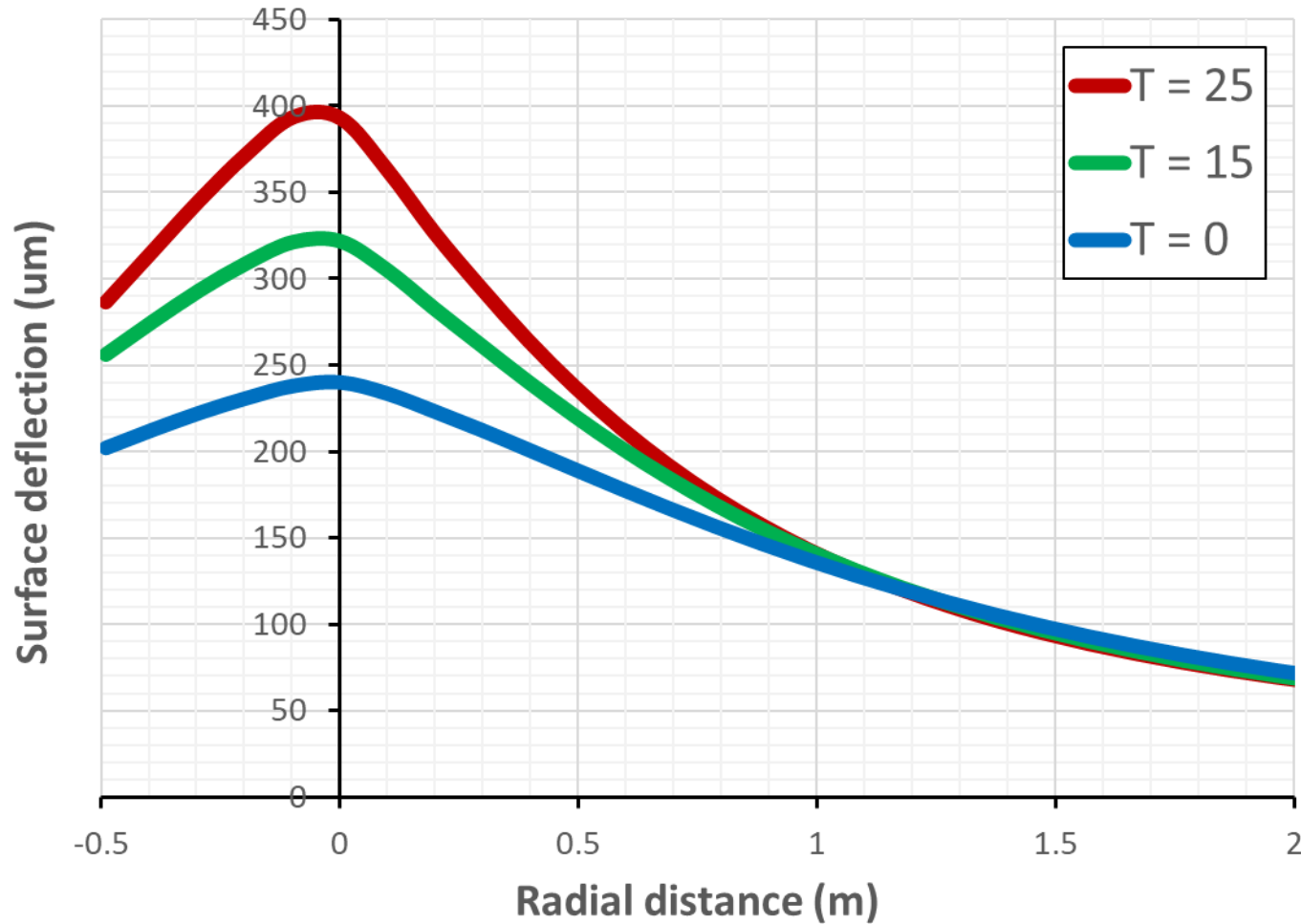


# Rutting model

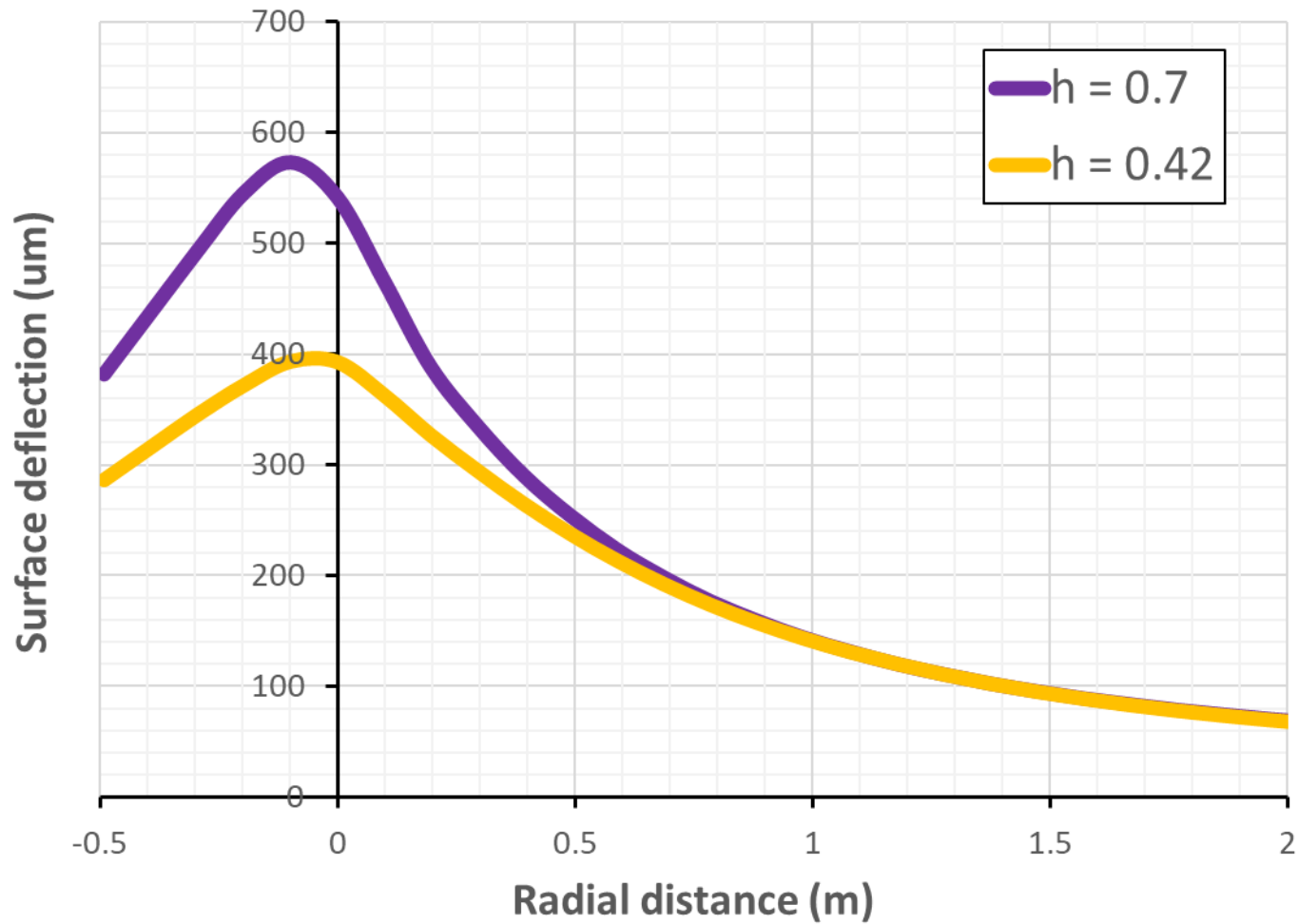
- Compressive strain at the mid point of layer 4



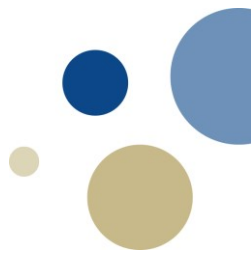
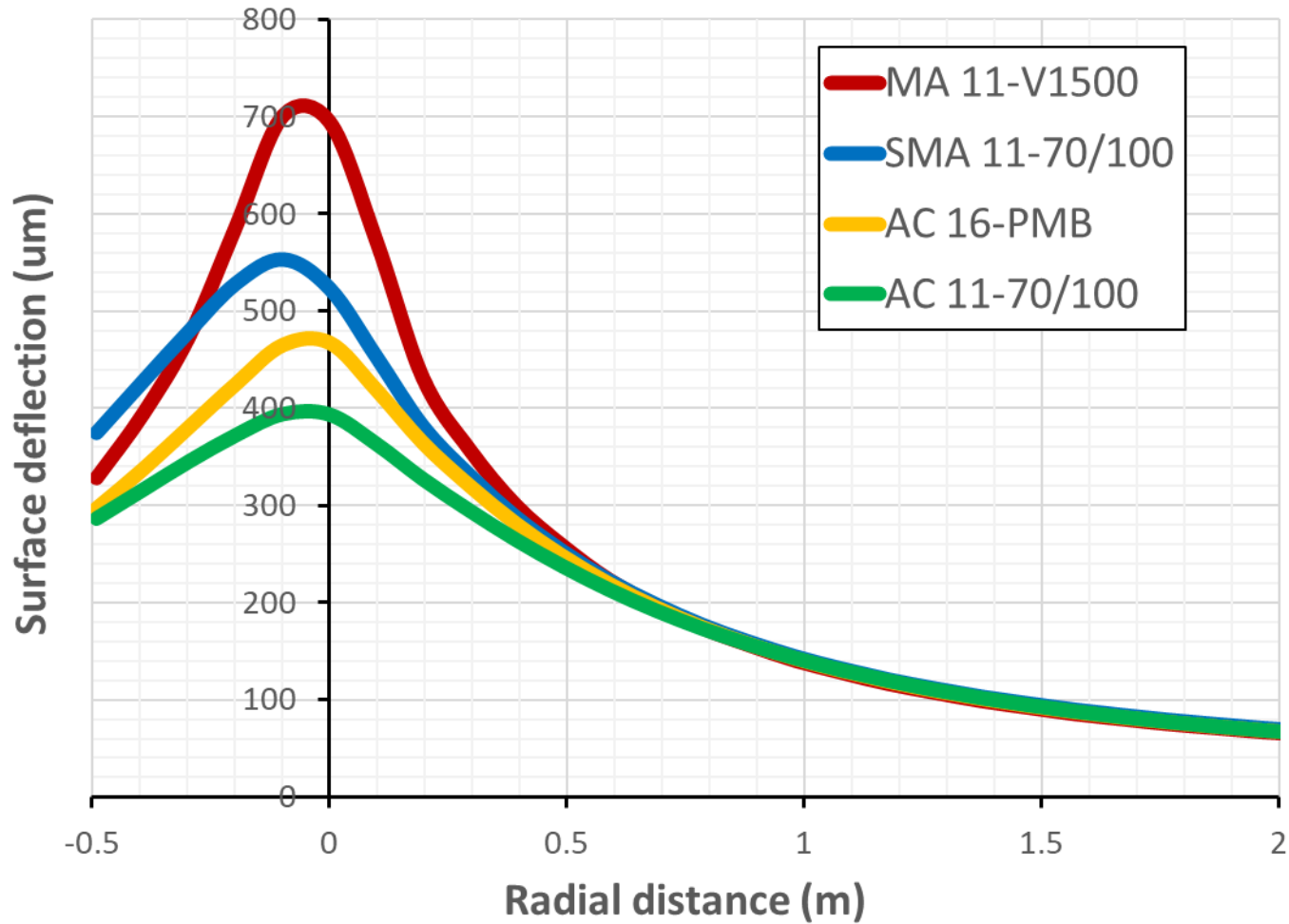
# Temperature difference



# Model parameters

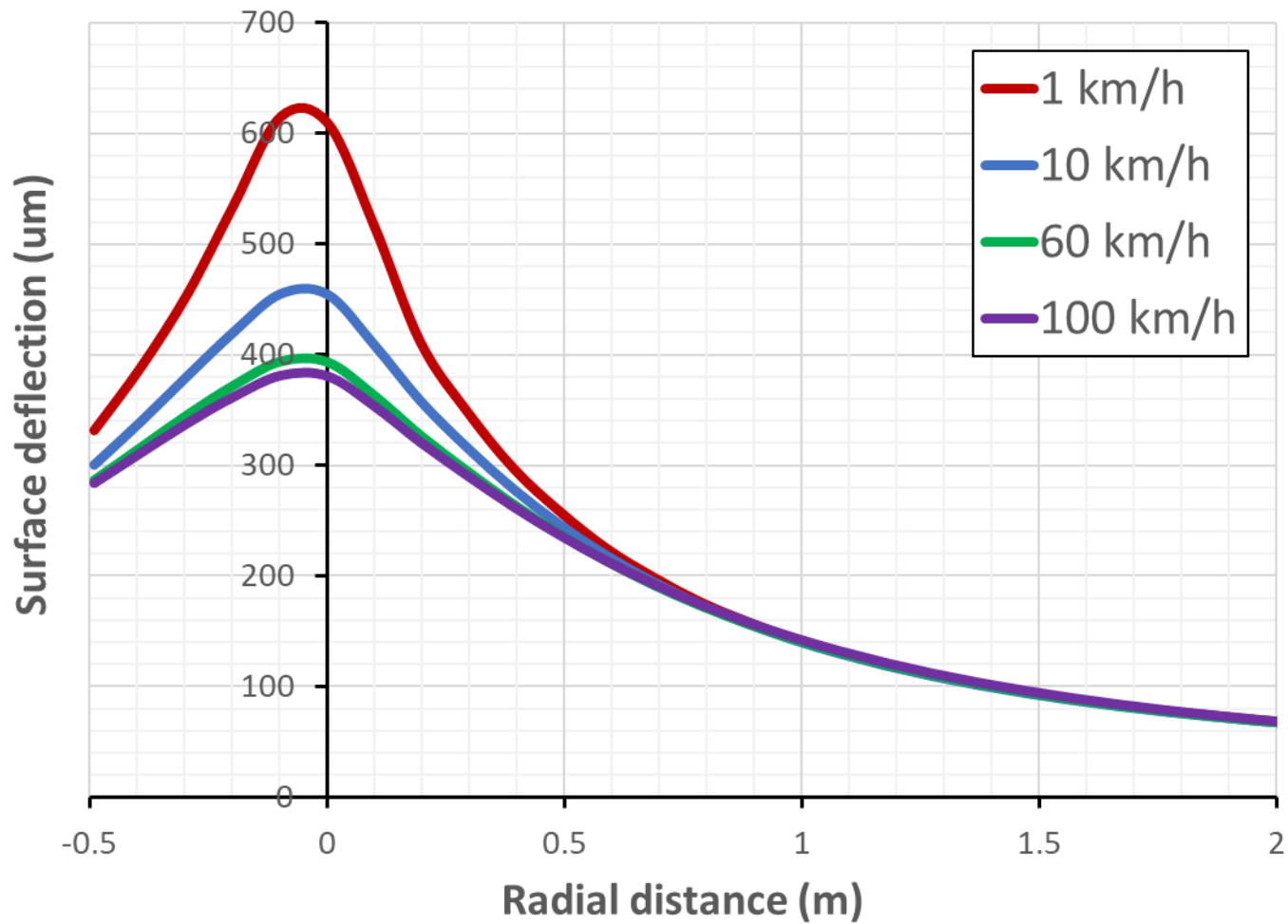


# Mixture type



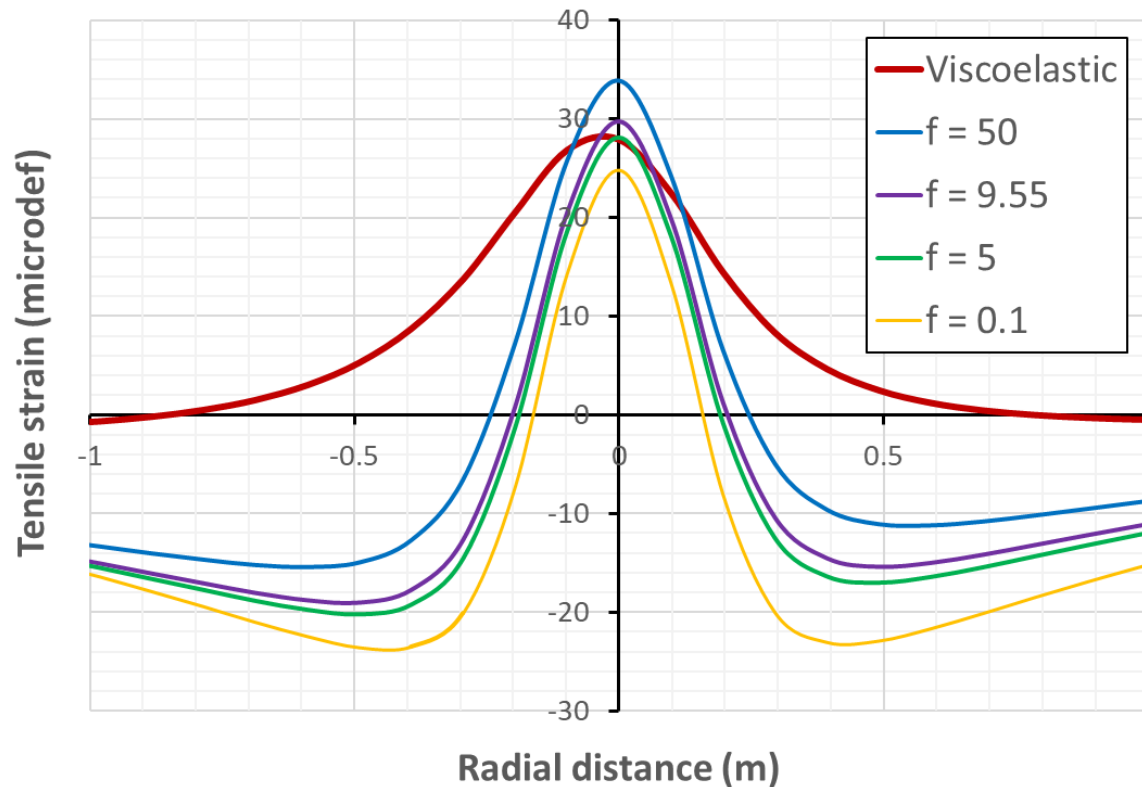


# Driving speed



# Design frequency

- Tensile stress at the bottom of asphalt layers



# Conclusion

- Repeatability of TSD and Raptor
- A good correlation between TSD and FWD
- Regression models between TSDDs and FWD can be defined
- Correcting Raptor data increases consistency with FWD in determining bearing capacity
- Raptor data should not be used in elastic back-calculation prior to refinement
- Regression correction models might not be unique
- Viscoelastic characteristics must be considered

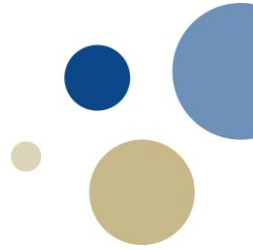


# Future studies

- Incorporating a viscoelastic analysis into ERAPave software
- Relationship between model parameters and deflection slopes of TSDDs should be established
- Determining deflection slopes from Raptor
- A more accurate procedure for obtaining deflections from deflection slopes should be obtained
- A temperature correction factor for TSDDs can be defined
- A speed correction factor for TSDDs can be obtained
- A more accurate formula for design frequency can be defined
- A new viscoelastic back-calculation procedure for obtaining pavement layers' moduli from TSDDs can be developed



# Thank you



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